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INVESTIGATING COMMITTEE REPORT TEST AVAND S2, RUN S2-212-B4-01

SYCAMORE TEST BASE

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FOREWORD

This document has been prepared under the direction of the Steering Committee for the Investigation of Test Stand S2, Run S2-212-B4-O1, and represents the common agreement of the participating agencies.

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FINAL ACCIDENT REPORT RUN S2-212-B4-01

1.0 ITERODUCTION

- 1.1 An explosion occurred at Sycamore Test Stand S-2 on 18 June 1958.

 during static firing test S2-212-B4-Ol (Run 212) on Missile 1B.

 No personnel were injured. Extensive hardware damage sustained by the following vajor components necessitated their removal and replacement: Booster Engine, Sustainer Engine, that portion of the Vernier engine contained within the thrust section. The jettisonable thrust section required repair. A preliminary investigation report was issued 20 June 1958.
- 1.2 In compliance with Convair DSP 1-29 an investigation was conducted to determine:
 - 1) The cause of the explosion .
 - 2) A means to prevent recurrence
 - 3) Extent of damage
 - 4.) A course of action which would provide the least interruption to the "B" series test program.
- The cause of the explosion has been determined. To prevent recurrence, recommendations have been proposed and corrective action has been taken. The missile was removed from the stand and transported to San Diego Plant Number 1 on 27 June. Repairs and replacements were effected by Sycsmore engineers and technicians under the provisions of Convair Cost Proposal 758-61, "Restoration of missile 1B and related TGSE at Sycamore Stand S-2 to Test Configuration," dated 9 July 1958. The missile was repaired and returned to Sycamore on 9 July.
- 1.4 The preceding page presents the membership of the Steering Committee, the Investigation Board and the Sub-Committees responsible for the compilation and documentation of this report.

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2.0 TEST CONDITIONS

- 2.1 Run S2-212-B4-01 (Run 212) was the fourth attempt to accomplish the fourth scheduled test on Missile 1B. The three previous attempts were prematurely terminated as follows:
- 2.1.1 Run S2-209-B4-01 (Run 209) was terminated, after 1.18 seconds, by the Sustainer overspeed control circuit.
- 2.1.2 Run S2-210-B4-01 (Run 210) was terminated, after 3.4 seconds, by a manual cutoff when missile LO₂ tank pressure fell below Redline limits due to failure of a solenoid operated check valve in the Airborne He bottle charge line.
- 2.1.3 Run S2-211-B4-O1 (Run 211) was terminated, after 1.1 seconds, by the Sustainer overspeed control circuit.
- Runs S2-203-A2-01 and S2-205-A2-01 in the first block of the 1B test series were also prematurely terminated by the Sustainer overspeed control circuit. Since recorded engine parameters reflected no indiation of turbine overspeed in any of the four instances of overspeed cutoff, it was resolved that these cutoffs were due to overspeed trip malfunction. In order to prevent a recurrence in Run 212, the overspeed control circuit was disconnected at the engine relay box. Turbine speed was monitored on a Brown recorder and the Sustainer LO2 Reference Regulator setting was reduced to 785 PSIG from 810 PSIG in order to decrease the rate of thrust build-up in the event it became necessary to execute a manual cutoff.
- 2.3 Run 212 scheduled engine durations were Booster 100 seconds, Sustainer 194 seconds and Vernier 220.5 seconds.
- 2.4 The primary objectives of Run 212 were:
 - (1) Analyze the performance of the MA-1 Propulsion System during a long duration three stage engine firing with programmed gimbaling in each stage, (2) Analyze the operation of the Airborne Pneumatic system, (3) Develop Series "B" tanking and starting techniques and, (4) Develop procedures for systems checkouts and "B" series static firing in support of operations at AFMIC. For detailed description of test objectives see General Captive Test Plan No. ZB-7-036, Revision B.
- 2.5 Booster and Sustainer staging were to have been initiated by the Flight Programmer. Missile hydraulic requirements were to have been supplied by the Airborne System. Missile pneumatics were to have been supplied by the Airborne system with continuous replenishment from the facility helium system. However, switchover to Airborne engine control pneumatics did not occur due to premature cutoff. Missile electrical requirements were to have been supplied by the Airborne battery and inverter, however, they were supplied from the ground system because Airborne battery voltage was too high.



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- 2.6 Run 212 was performed in accordance with "Run 4 countdown 17 June 1958."
 This countdown deviated from the countdown signed off by the design groups on 3 June 1958 as follows:
- 2.6.1 The fuel tanking level of 10,761 gallons was changed to 10,766 gallons in order to comply with report AA-E-130, Propellant loading for the XSM-65-B3 Missile.
- 2.6.2 Due to failure of the PU manometers LO₂ was dumped to missile station 519, according to Vibrotron readings, instead of to a computer comparator null error indication.
- 2.6.3 Because the allowable temperature at the LO₂ breakaway valve (PlO2IT) was exceeded during Runs 209 and 210, the 60 second time count was eliminated. All the items in the 60 second count were re-sequenced to move the LO₂ dump to within 30 seconds of major command "Vernier Squibs Fire" (Time Zero). Commands were called out by the Test Conductor and a 15 second time count was called out between commands "Depress Start Switch" and "Vernier Squibs Fire."
- 2.6.4 Run 4 countdown dated 17 June 1958 is included in this report as Appendix A. The only deviation from this countdown during Run 212 was that missile power was supplied from external because the internal missile DC power system malfunctioned.

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FINAL ACCIDENT REPORT RUN S2-212-B4-01

3.0 TEST PREPARATIONS

3.1 X-1 Day Preparations

X-1 day preparations began at 2400 17 June and were completed at approximately 1400 18 June. Fuel remained on board the missile from the previous day's run attempt and the missile was in a state of readiness which considerably reduced the preparations required.

- 0020 The fuel tank was topped off to station 953 as indicated by the sight gage. The flow total registered 80 gallons of fuel tanked.
- 1200 Booster and Sustainer engines were Trichlor flushed and the Boosters were filled with lithium chloride.

1300-1400 - Igniters installed.

3.2 Precount Operations

- 1408 Precount operations started.
- 1451 An official hold was called. Inspection of the thrust section revealed grease around B2 thrust chamber gimbal mount. The area was cleaned & operations resumed. Total hold time was 14 minutes.
- 1510-1525 Precount operations were delayed to complete the installation of the flexible firewall.
- 1530 Transfer of LN_2 to the missile shrouds started.
- 1556 All shrouds were filled and the LN2 flow control valves had cycled.
- 1556 Precount operations were completed. Predicted duration for this section was 60 minutes; actual elapsed time was 108 minutes.

3.3 Countdown Operations

- 1600 Countdown operations began and the area was placed in Condition Red.
- 1601 Booster and Sustainer hydraulic systems set up started. The Sustainer missile return pressure was reported to be 7 psig. A hold was called at 1602 to send a mechanic to the area to check the return gage on the Sustainer hydraulic cart. It indicated 6-8 psig. By use of the hand pump in the cart, the pressure was increased to 33 psig. It then dropped slightly, stabilizing at about 28 psig. Countdown operations resumed at 1608 after a total hold of 7 minutes.



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3.3 (Cont'd)

- 1608 Missile bottle pressurization commenced. Instrumentation reported a bottle pressure of 3000 psig at 1611.
- 1609 Missile pressurization Sequence 2 was initiated.
- 1609 LO, tank and facility chilldown commenced.
- 1616 Pumps IA & LB were started. LO₂ tanking was switched to a separate communications channel and LO₂ was tanked according to the support requirements of missile 3B.
- 1633 Missile pressurization Sequence 3 was initiated.
- 1637 Missile power was switched to internal. Upon switching DC, missile AC voltage and frequency increased rapidly out of limits and the DC internal voltage was reported to be approximately 34 volts. It was decided to continue the run on external power. Post run investigation of records revealed that the missile battery had not been pre-loaded by the factory.
- 1637 At approximately X-57 seconds, LO₂ was dumped for 27 seconds to missile stateion 519.
- 1638 Booster and Sustainer ignition was initiated. Immediately after ignition, cutoff occurred and fire was reported in the thrust section. All firex systems were turned on and the fire quickly extinguished. Booster Ground Bus Power and Booster Engine Control pressure was lost. All power to the missile was secured.
- 1642 CO2 system secured.
- 1642 LO2 detanking commenced.
- 1655 Fire was reported again in the thrust section. The CO₂ system was turned on and the fire was quickly extinguished.
- 1657 The COp system was again secured.
- 1713 LO, detanking was completed and the firex system was secured.
- 1715 An attempt was made to detank fuel but the tank observers reported heavy leakage from the thrust section and it was decided to leave the fuel in the missile until an investigation could be made. Upon reporting to the area, the Stand Engineer reported heavy thrust section damage and fuel leaking downstream of the Sustainer pre-valve. After further investigation of damage to the missile, the Sustainer pre-valve was kept closed by removing the opening control pressure line, and the fuel was detanked.

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FINAL ACCIDENT REPORT RUN S2-212-B4-01

3.3 (Cont'd)

1745 - All systems were secured. Predicted durations of this section was 80 minutes; actual elapsed time was 105 minutes.

3.4 Safety Precautions

Safety Engineer Report -- Sycamore Test Site

- 3.4.1 The X-1 day and precount preparations were accomplished with proper safety precautions. Supervision in all sections carried out their sheeduled work assignments with proper safety equipment. Coordination between Stand area and Blockhouse key personnel was satisfactory in all phases of countdown.
- 3.4.2 During the attempted firing all personnel assigned to specified tasks were at their stations and in direct contact with the Test Conductor's area. They carried out these tasks in an orderly and well coordinated menner.
- 3.4.3 Immediately after the accidnet exceptional team effort was shown by all personnel. I believe it was this team coordinated effort that held the damage to this limited extent.

R. H. Moore Safety Engineer

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- 4.1 The following is a summary of visual observations made before, during and after the explosion based on written testimony of Blockhouse and Tank Observers. Where these observations were not substantiated by test data a qualifying comment is added.
- 4.1.1 V2 Ignition appeared normal. V1 ignition appeared fuel rich and rough. However, test data does not substantiate a rough fuel rich V1 ignition.
- Booster and Sustainer ignition appeared short. A puff of smoke was immediately noticed to come from the Sustainer engine and fire broke out, concentrated primarily in the region of the Sustainer and Bl exhausts. A spreading fire was seen near the VI flame deflector which became entrained in the flames bellowing up from the lower thrust section.

Review of photographic coverage and hardware investigation reveals no indication of fire in the region of the VI thrust chambers.

- 4.1.3 Fire was reported by observers within 7 seconds of Vernier ignition and was also noted on the Blockhouse television display at this time. CO₂ firex and launcher coolant systems came on and the fire was promptly extinguished. CO₂ was turned off and the firex was left on.
- 4.1.4 A second flare up was observed and promptly extinguished by again turning on CO₂. Fire and launcher coolant systems remained on throughout the fire.
- 4.1.5 CO₂ was turned off and detanking of LO₂ was accomplished without incident. The stand engineer and a fireman were sent out to inspect the missile. Firex and launcher coolant systems were turned off.
- 4.1.6 When the fuel prevalves were actuated to detank fuel, considerable fuel appeared to be coming from the Sustainer Gas Generator exhaust. Detanking of fuel was delayed until the Sustainer fuel prevalve control could be disconnected.
- 4.1.7 Post run hardware examination revealed that the Sustainer Gas Generator Fuel blade valve remained closed throughout the run and that the fuel blade valve seals were intact. It was also determined that the fuel volute of the Sustainer turbopump contained a crack approximately 3/8" X 10". It is therefore believed that the fuel reported by the observer as leaking from the Gas Generator exhaust was actually coming from the cracks in the fuel turbopump volute.
- 4.1.8 Verbatim testimony of the observers is presented as Appendix B to this report.

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FINAL ACCIDENT REPORT RUN S2-212-B4-01

5.0 TEST DATA

The following is a chronological presentation of significant Run 212 data analysis as pertains to the cause and history of the thrust section explosion which occurred during this run. The time at which each event occurred is stated in seconds with relation to Vernier Igniters Firing (Zero Time). Appendix C of this report gives a detailed presentation of the analysis of all data recorded during Run 212. Appendix D presents a detailed chronological history of significant data. (Appendices C and D follow Section 7 of this report).

5.2 Chronological History of Major Events:

(Zero time is Vernier Igniters firing)

TIME (SECONDS)	EVENT
-467	Sustainer Gas Generator discharge temperature indicates a decline from 117 Deg. F to negative peg. The time at which this decline took place is unknown as the recorder was not turned on until -467 seconds.
-299.83	Commenced pressurization Sequence III which indicates the LO ₂ tanking was completed.
-149.13 to -90	During this period, three unsuccessfull attempts were made to switch electrical power to internal and the run proceeded on external power.
-61	Indication of continuous LO ₂ flow of approximately 3 lbs/min to the Sustainer Gas Generator. The time the flow started is unknown as the CEC recorder No. 8146 was not turned on until this time.
-38.13	LO ₂ duct pressure activity indicating fill and drain valve closing at completion of LO ₂ dumping.
-13.24 to -1384	Vernier start sequence initiated and start tanks pressurized resulting in transient Vernier and Gas Generator propellant flows due to displacement of gas. Sustainer Gas Generator LO ₂ flow increases to .5 lbs/minute (See Graphs 6, 8 & 10)
0	Vernier igniter squibs signaled to fire.
64 to 0.83	Vernier propellant valves signaled to open, propellant and chamber pressures indicate combustion occurs (See Graphs 1, 2 & 6).
-0.84 to 0.89	Sustainer gas generator fuel flowmeter indicates low amplitude signal or noise which may indicate

(See Graph 9).

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flow to gas generator or igniter fuel valve.

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5-2 (Cont'd)

TIME	EVENT
1.81 to 1.82	Booster and Sustainer LO2 and igniter fuel valves energized to open indicating main igniters have fired.
1.87 to 2.22	Booster and Sustainer main LO, valves open; pressures and flows indicate igniter LO, and fuel flow (See Appendix D). Sustainer gas generator fuel flow indication may be flow to gas generator. (See Graph 9).
2:30	Ignition complete indicates ignition detection signaled gas generator igniters to fire.
2.31 to 2.37	Many measurements indicate transients or loss of signal. (See Appendix E). Booster and Vernier sequence control power is lost indicating disruption of electrical circuits. Loss of ground automatically initiates cutoff. Load cells and launcher strains indicate shock of significant magnitude (See Graphs 3 & 5). Most accurate time correlation is by measurements recorded on oscillograph which indicate shock originated in Sustainer section. Sustainer fuel flow starts at 130 lbs/sec. indicating system ruptured. (See Graph 7).
2.38 to 2.47	Engine compartment temperature starts to increase though not abnormally (See Graph 11). Other measurements indicate transients and loss of signal.
2.48 to 2.53	Vernier pressures indicate propellant valves closed and combustion ceasing.
2.65	Sustainer HSV closed by microswitch indication but still partially open by angular position transducer.
2.74 to 3.01	Many measurements still erratic and losing signals
3.27 to 3.31	Missile movement, Sustainer fuel duct pressure, activity and engine compartment temperature and launcher strains indicate another shock and probable start of major fire (See Graph 5).
3.42	Sustainer HSV confirmed to be closed by angular position, transducer. This indicates electrical control circuit disruption since the open signal and control hydraulic pressure were still present.
5.08 to 5.21	Engine electrical control circuits de-energized by cutoff; propellant start tanks vent.

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EVENT

5.2 (Cont'd)

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7.87 to 7.97	Missile movement and pneumatic pressure transients indicate another shock or airborne pressure supply transient.
13.36 to 17.87	Propellant pre-valves indicate closed and Sustainer fuel flow ceases (See Graph 7)
20.67 to 30	Thrust section temperatures reach maximum and begin to decrease towards ambient (See Graphs 11 & 14) indicating fire decreasing.
48.87	Fuel tank pressure indicates restep to Sequence II.
120	Thrust section temperatures at or near ambient indicating fire out. (See Graphs 11 & 14).

5.3 Analysis of Results

TIME

5.3.1 Propulsion System:

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- 5.3.1.1 The Sustainer gas generator temperature (Graph 19) and lox flowmeter (Graph 8) indicate lox flowing into the combustor prior to start. Indicated fuel flow to the Sustainer gas generator (Graph 9) is suspected as signal noise because of the low amplitude, non-sinusoidal trace.
- 5.3.1.2 Vernier ignition and start tank fed operation were similar to previous runs. (Graphs 1, 2 & 6). Main engine ignition was completed but mainstage was not achieved due to lack of gas generator igniter links break signal. Without the GG igniter links break signal the gas generators propellant blade valves and main fuel valves were not signalled to open. Vernier propellant and main lox valve closed, apparently due to loss of electrical control power as opening signals were still transmitted until 2.78 sec. after ignition was completed. Cutoff vented the start tanks. Sustainer fuel flowed for 13 sec. from ignition complete until propellant pre-valves closed, indicating that the Sustainer fuel system was ruptured as there was no indication of fuel valves opening.
- 5.3.1.3 Analysis of records from the preceeding firing, Run 211, show a pronounced temperature surge in the Sustainer Gas Generator immediately after cutoff. (See Graph 20). Temperature rose from approximately 1000° at cutoff to 1800° 0.1 second later. The recorder pegged at 1820°F for 0.5 seconds, fell to 1450°F, spiked to 1680°F, and then declined normally. After the run the transducer was inspected and showed evidence of being burned and was replaced prior to Run S2-212. This measurement has not been reliable in the past, and the above temperatures can be considered approximate only, in view of the damage

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FINAL ACCIDENT REPORT CONFIDENTIAL RUN S2-212-B4-01.

- suffered by the transducer. However, it is reasonable to conclude that a large and relatively prolonged temperature surge occurred immediately after cutoff. This surge probably caused the failure of the Ges Generator LO₂ seals. It represents the only significant deviation from normal run conditions, disregarding Sustainer Overspeed Trip activation, which was observed in Run 211 data.
- 5.3.1.4 The Sustainer Gas Generator was disassembled at Sycamore. The blade valves were found in the closed position. The LO₂ seals were shattered. The fuel seals were intact (See photographs 17 through 28).
- 5.3.1.5 After examination of the Sustainer Gas Generator at Sycamore the unit was released to Rocketdyne for examination at Canoga Park. A detailed examination of individual components was conducted. It was discovered that the injector head was bulged slightly downward (068 inches maximum). The LO₂ manifold was found to be slightly bulged upward and outward (.020 inches). (See Appendix F for Rocketdyne reports).
- 5.3.2 Electrical System:

After three attempts to switch to internal electrical power, the electrical power remained on external and was normal until 2.36 sec. when propulsion control power (ElO27V) indication was lost; missile systems power remained normal for remainder of the test.

5.3.3 Pneumatic System

Propellant tank pressures were normal throughout the test. Fuel tank and lox regulator pressures reflect change to internal at approx. -31 sec, but temperatures do not reflect cold gas flow. Sustainer control pressure transient (@2.27 sec), indicates controls pressure switchover to internal .71 after this signal. Most measurements indicate signal loss or transients after ignition complete (2.30 sec.) as result of shock, fire, and disruption of instrument signal circuits. Indicated booster control pressure loss is a signal loss as LO₂ reference regulator still indicates pressure.

5.3.4 Fydraulic System

Ground supply maintained pressures satisfactorily.

5.3.5 Flight Control System

Engines were maintained in null position, autopilot program was not initiated as main engines complete signal was not transmitted.

FINAL ACCIDENT REPORT CONFIDENTIAL RUN S2-212-B4-01.

- 5.3.1.3 (Cont'd)
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5.3.5 Flight Control System

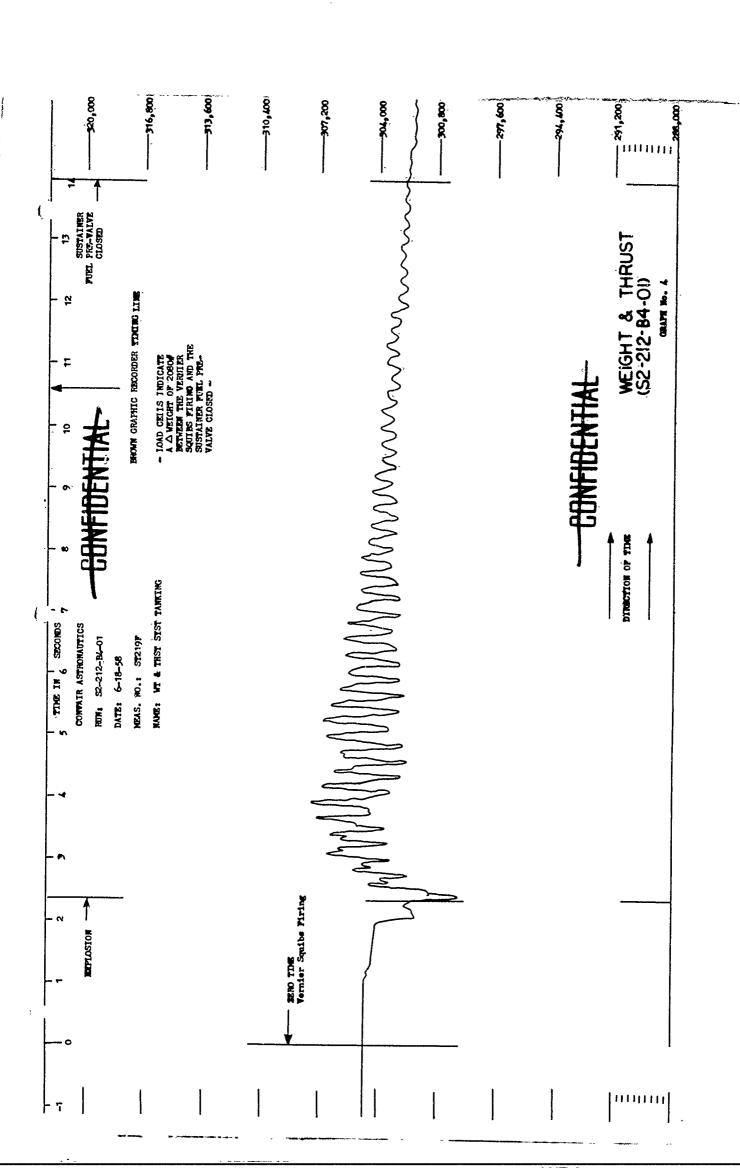
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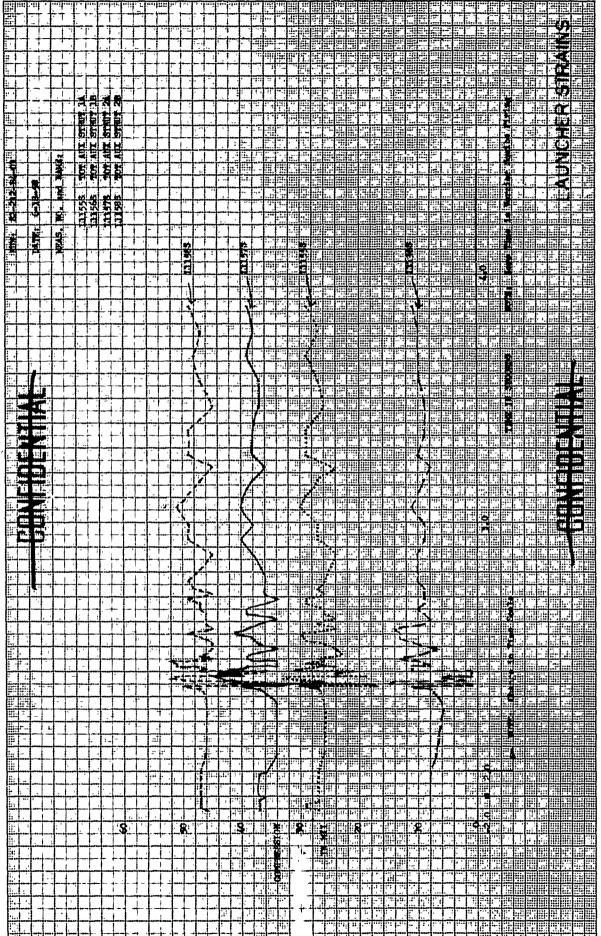
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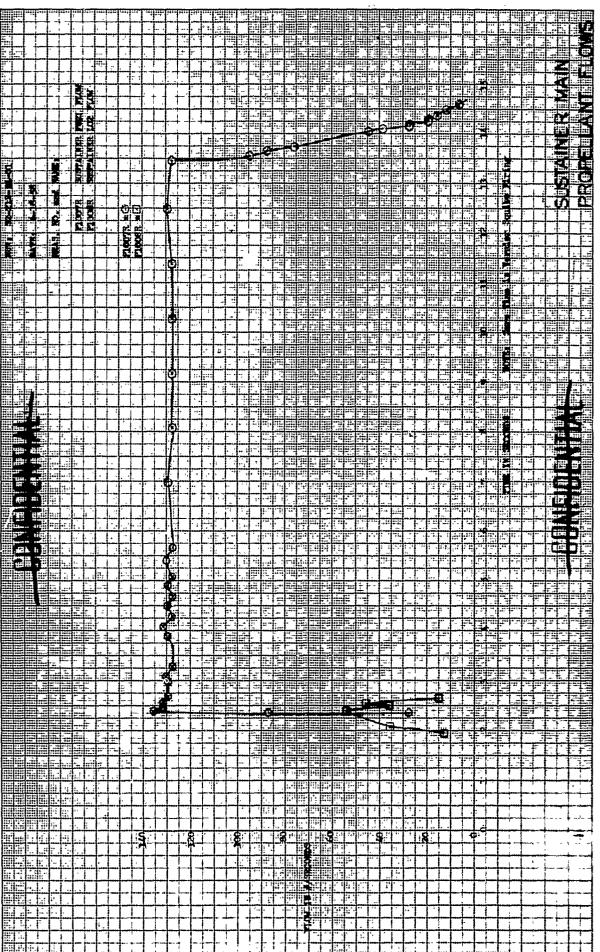
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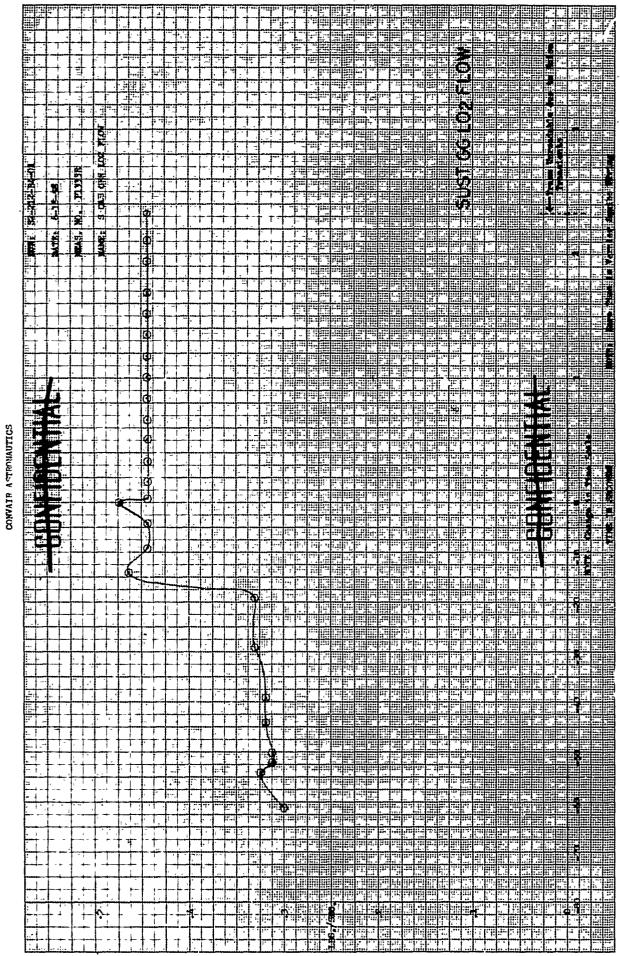




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GRAPH No. 16

CONVAIR ASTRONAUTICS

CRAPH No. 17

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CRUPH No. 18

CONVAIR ASTRONAUTICS

FINAL ACCIDENT REPORT RUN S2-212-B4-O1 2000 900 800 700 600 500 400 S GG FUEL BLADE VALVE INLET PRESS. P1280P 300 200 100 X+4 X+3 X+2 X+1 X-1 X-2 TIME (SEC) GRAPH 21 DIRECT REPRODUCTION

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CONFIDENTIAL FINAL ACCIDENT REPORT RUN S2-212-84-01

6.0 HARDWARE DAMAGE

6.1 The following is a summary of the hardware damage sustained by Missile 1B as a result of the explosion in the Sustainer turbine system.

6.2 Sustainer Engine

- 1) Nozzle and second stage turbine wheel blown off (See Photo 6).
- 2) Fuel pump volute cracked completely around circumference. Also crack approximately 10 inches long and 3/8 inches wide near hub. (See Photo 5).
- 3) Turbo pump gear case separated. (See Photos 5 and 28).
- 4) Gas Generator exhaust shroud torn off and blown upward toward Quads I and II (See Photos 1 and 7).
- 5) Exhaust shroud straps torn off and hanging loose. (See Photo 1).
- 6) Thrust chamber torn and twisted, tubes sheared from throat section downward. Primary force was applied from Quad IV to Quad II with heaviest damage at fourth band down from throat. Chamber bands were "U" shaped and exterior of Quad IV was compressed to interior of Quad II. (See Photos 1 and 2).
- 7) Three cannon connectors were broken on Engine Relay box. Bottom of Relay box slightly bent around connector.
- 8) All drain lines were bent, twisted, and collapsed (See Photo 2).
- 9) Exhaust manifold blown out through flame bucket. One small section imbedded in skirt section at Quad IV. (See Photo 6)
- 10) Sustainer Gas Generator Number PO86 (NAA 9512-44185-51) was removed and analyzed to determine the condition of the blade valves and combustion chamber. Results of the investigation disclosed the LO2 downstream port seal was shattered and the upstream seal was cracked. (See Photos 17 through 28).

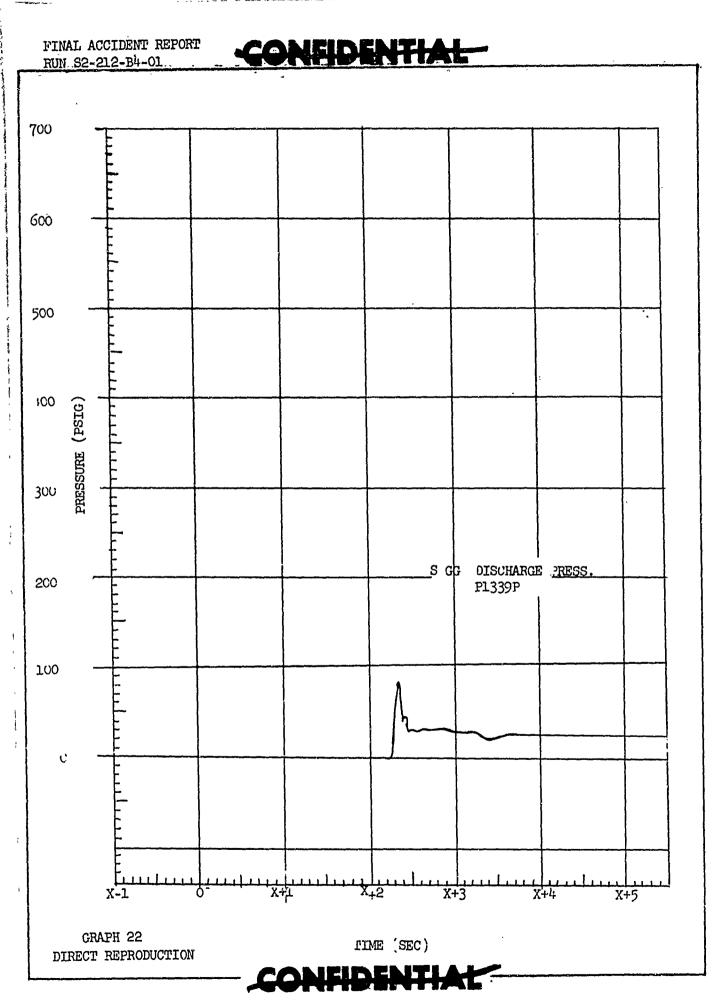
6.3 Booster Engine

- 6.3.1 Bl Thrust Chamber Damaged beyond repair (See Photos 8 and 9).
 - 1) Quad II damage consisted of an 8 inch cut 2 feet from the bottom, and a $1/\mu$ inch hole 1 foot from the bottom of the thrust chamber.
 - 2) Between Quads II and III damage consisted of a large 6 inch conceive area with a 2 inch hole through the wall 3 feet from the bottom, eight smaller holes and concave areas, and a 1/2 inch hole through the wall.



6.3.1 (Cont'd)

- 3) Demage in Quad III consisted of two 2 inch holes approximately 2 feet from bottom of chamber, a 2 inch cut and a small hole through the wall 3 feet from the bottom, a 1/2 inch hole and twelve collapsed tubes 1 foot from the bottom, a 1/2 inch hole 7 inches from the bottom, and three small dents 3 inches from the bottom.
- 6.3.2 Bi Thrust shander Heavily damaged (See Pastos 10 and 11).
 - 1) Damage consisted of punctured tubes and 1/2 inch holes between second and third bands of chamber, a 6 by 14 inch concave area and collapsed tubes between third and fourth bands on side toward Sustainer. The area was dented diagonally for 3 inches. In addition, eight tubes were sheared off.
- 6.3.3 Booster Engine Components
 - 1) Miscellaneous engine plumbing destroyed (See Photo 2).
 - 2) Booster turbine exhaust duct below heat exchanger collapsed. (See Photos 3 and 7).
 - 3) Lube oil tank punctured. (See Photo 4).
 - h) Pneumatic control system damaged extensively.
 - 5) An estimated 90% of all eagine or first viring destroyed.
- 6.4 Vernier Engine No. 1
- 6.4.1 Damage to the V-1 engine consisted of the following:
 - 1). Pressure switch harness burned.
 - 2) Pitch actuator berness burned.
 - 3) Several wires in Plug P90208-7 were charred and potting compound around plug was melted.
 - 4) Ground wire to Receptable 390208-7, and several other wires were charred.
- 6.5 Thrust Section (See Farto 14)
- 6.5.1 Demaye in Quad I
 - 1) Interskin and compression strut pulled loose at Sta 1248.
 - 2) Interskin pulled loose 75 inches from Quad I between Sta 1248 and 1297.
 - 3) Skirt section pulled loose from rivets in barrel section between Sta 1297 and Sta 1248.



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- 4) Horizontal strut and bulkhead at Sta 1268 pulled from rivets. Bulkhead rippled.
- 5) Strut between Sta 1297 and Sta 1268 pulled loose with some corrugation.
- 6) Bulkhead web at Sta 1248 pulled loose from rivets and bulkhead rippled.
- 7) Bulkhead web at Sta 1297 pulled loose at rivets.
- 6.5.2 Damage from Quad I to Quad II
 - 1) Split along rivets in thrust barrel section at Sta 1268.
 - 2) Dents (35) ranging from 9 to 15 inches from end of barrel between each corrugation.
 - 3) Interskin pulled loose from rivets at Sta 1297 bulkhead.
 - 4) Interskin pulled loose from rivets at Sta 1268.
 - 5) Interskin on X-X axis pulled loose from Sta 1248 to Sta 1297.
 - 6) Interskin pulled loose from rivets at Sta 1297 bulkhead.
 - 7) LN2 fill and drain line damaged by 2 inch hole at Sta 1248.
- 6.5.3 Damage in Quad II
 - 1) Tubing badly burned.
 - 2) Interskin pulled loose 15 inches from Quad II between Sta 1206 and Sta 1297.
 - 3) Corrugation pulled loose from Sta 1297 bulkhead.
- 6.5.4 Damage from Quad III to Quad IV
 - 1) Bulkhead web at Sta 1299 torn loose from rivets. Eight feet of Web torn in many places.
 - 2) Innerskin riveted to corrugation from Sta 1268 to Sta 1299 torn loose. Multiple cracks in innerskin and rivets pulled out.
 - 3) Innerskin riveted to corrugation from Sta 1268 torn loose. Rivets pulled out and stiffeners cracked.
 - 4) Corrugation of Sta 1248, halfway between Quads, torn loose from rivets.



6.5.4 (Cont'd)

- 5) Launcher purge and control panel between Quads at Sta 1300 demated and twisted. (See Photo 13).
- 6.5.5 Damage in Quad IV (See Photos 12, 15 and 16)
 - 1) Compression struts torn loose from mounting brackets at Sta 1245 and Sta 1280.
 - 2) Large diagonal hole, 12 by 4 inches, torn in corrugation of Booster pod extension at Sta 1287.
 - 3) Diagonal hole in 6 inch section of bulkhead at Sta. 1299.
 - 4) Disconnect panel (7-77260-1) at Sta 1268 disconnected and twisted.
 - 5) Corrugation at Sta 1299 torn loose by piece of Sustainer exhaust shroud. Corrugation extended about 12 inches.
 - 6) Bulkhead rivets at Sta 1299 pulled out. Web and angle web torn.
 - 7) Rivets pulled loose from corrugation at Sta. 1268. Corrugation and webbing torn across width and corrugation extended about 12 inches.
 - 8) Stiffener at Sta 1240 pulled out and a crack, about 10 inches, extends away from rivets.
 - 9) Innerskin riveted on corrugation, behind jettison rail from Sta 1206 to 1248, torn and pulled from rivets.
 - 10) Corrugation of Sta 1268 pulled from former bulkhead and extended from 1 to 12 inches away from center of thrust chamber.
 - 11) Vertical tear in inner skin along rivets between Sta 1230 and 1240 extends about 30 inches from X-X axis.
 - 12) Vertical tear in inner skin along rivets between Sta 1240 and Sta 1247 extends for about 15 inches from Y-Y axis.
 - 13) Thrust barrel parted from bulkhead at Sta 1268 for about 4 feet starting at X-X axis.
 - 14) Hole torn in thrust barrel structure on X-X axis.
 - 15) Hole torn in thrust barrel structure about 12 inches from X-X axis.
- 6.6 Thrust Section Interior
- 6.6.1 General Damage
 - 1) Heat exchanger dented for about 1/4 its circumference on side facing the Sustainer.

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6.6.1 (Cont'd)

- 2) Lower compression strut mounting bracket broken and piece missing.
- 3) Gusset (7-77961-38) bent and torn with one rivet popped out.
- 4) Angle strut (7-77961-34) bent and torn.
- 5) Entire area below bulkhead at Sta 1268 heat blistered.
- 6) CO₂ and Firex pipe bent and twisted in Quads I and IV. Firex pipe smashed into Bl, causing severe damage. (See Photo 9) Braces for Firex pipe bent and twisted.
- 7) Compression struts in Quads I and IV torn loose from thrust section skirt (both upper and lower strut). In Quad II, only the upper strut is loose. In Quad III, only the lower strut is loose.
- 8) LN2 supply line to pressurization bottle shroud caved-in directly below shroud in Quad I and II.
- 9) Bl engine relay box connectors burned and broken.
- 10) Split 3 inches long in bottom half of Booster lube oil tank on Quad IV side. (See Photo 4)
- 11) Lower Booster relay box bracket torn off.
- 12) Oval shaped crack about 12 by 8 inches in diameter in Sustainer turbopump gear case.
- 13) Crack in fuel volute of Sustainer turbopump. (See Photo 5).
- 14) Engine pneumatic manifold wiring charred and burned.
- 15) Booster exhaust duct caved-in below heat exchanger. Small dent in heat exchanger. (See Photo 7).
- 16) On lower Booster engine relay box, one cannon connector broken and 2 connectors burned and cracked. Cannon connector lines burned and cracked.
- 17) Asbestos on thrust section heating duct torn, twisted, and burned.

6.7 Missile Pods

- 6.7.1 Damage to equipment in Missile pods was as follows:
 - 1) Ground wire for MSD plug and Jll31 connector burned entire length (approx. 24 inches).
 - 2) Taped end of ground cable at base of pod burned approximately 3 inches.

7380

6.7.1 (Cont'd)

- 3) Potting compound for MSD cable and connector (J1131) charred 6 inches from connector.
- 4) Pod doors paint blistered in area 6 inches wide over entire length of doors.

6.8 Facilities

- 6.8.1 Damage to facility equipment was as follows:
 - 1) Rubber insulation from wire between Quads I and IV burned and melted along trunnion at level 17.
 - 2) Rubber insulation on wire at level 17 between Quads III and IV melted and burned.
 - 3) Leak in hydraulic flex line at rise-off fitting in Quad IV, level 17. (See Photo 13).
 - 4) All rise-off panel hydraulic flex lines between Quads III and IV at level 17 are badly discolored from smoke and burning.
 - 5) Flex heater duct across deck between Quads I and IV at level 17 burned for about 6 feet of its length.
 - 6) Foil wrapping on Pod coolant flex line in Quad IV, level 17, blown and tattered. Little evidence of flex line burning.

6.9 Tower

- 6.9.1 Damage to tower components and equipment was as follows:
 - 1) Curtain on south east side of tower at level 17 badly burned.
 - 2) Pod cooling duct between levels 17 and 27 scorched and burned for about 6 to 7 feet. All of one "Y" duct scorched and burned.
 - 3) Paint was badly scorched on southeast bottom side of tower level 35 platform.
 - 4) Paint on south bottom sides of tower level 27 platforms badly scorched and damaged by water.
 - 5) Thrust barrel heater ducting at level 17 badly scorched and burned in several places.
 - 6) Fence, railing, and duckboards on level 17 badly corroded and damaged by fire and water.
 - 7) CO piping south side of level 17 badly corroded and damaged by fire and water.

CONTIDENT AL FINAL ACCIDENT REPORT

6.10 Instrumentation

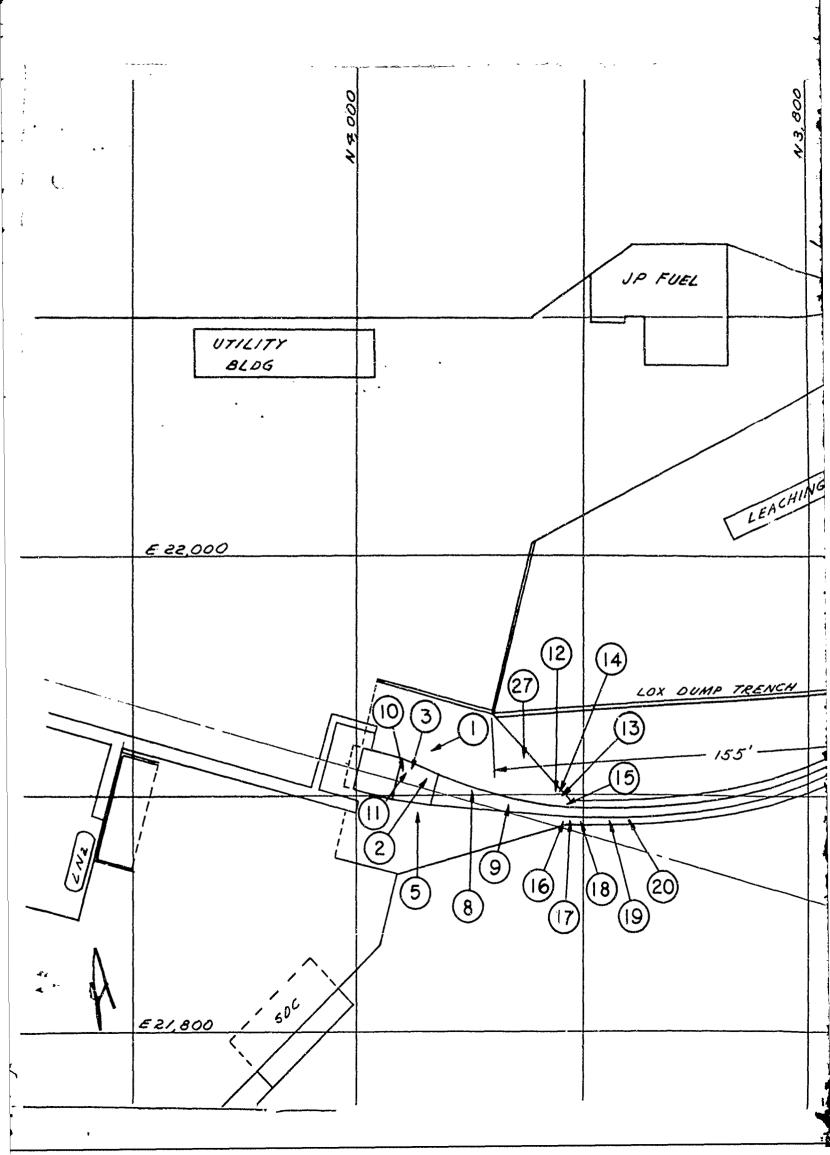
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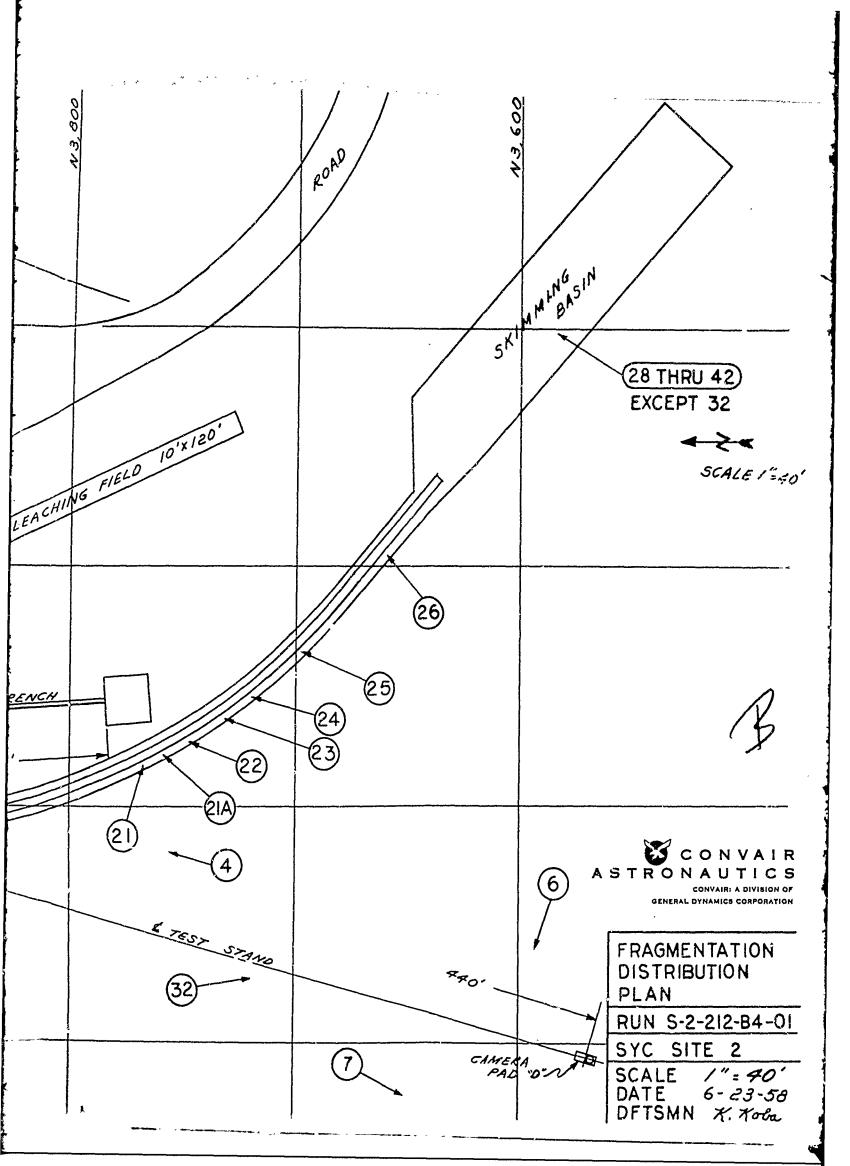
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AlogP	FAIRING DIFFERENTIAL	7-01225-805	204
F1011P	LO PRESS REG DISCH	7-01225-803	57
F1114P	LOS PRESS REG INLET	7-01226-801	148
F1124P	s Tank he btl disch	7-01226-801	267
H1.033P	Bl HYD ACCUMULATOR	7-01226-801	246
H1.052P	S HYD ACCUMULATOR	7-01226-5	13
H 1T	MSL HYD PUMP DISCH	7-01223-5	67
P1349B	S PUMP SPEED	7-01437-AL	NAA
P 2P	BL FUEL PUMP INLET	7-01226-1	15
Plolop (Bl LUB OIL MAN	7-01226-3	136
P1027P	VERNIER FUEL TANK	7-01226-3	442
P1059P /	B2 THRUST CHAMBER	7-01627-5	2297
P1091P	Bl LO ₂ INJ MAN	7-01627-801	2027
P1093P	Bl fuel inj man	7-01627-801	3534
P1094P /	B2 FUEL INJ MAN	7-01627-801	1763
P1235P '	VERN LOO TK REG OUT	7-01226-3	46
P1280P	s gg fuël vlv inlet	7-01226-3	65
P1330P	S FUEL PUMP DISCH	7-01226-801	50
P1332P	S LO ₂ PUMP DISCH	7-01226-801	50 5 3 52
P1489P	b cas cen lo ₂ viv in	7-01.226-3	3
P1014T	eng comp ambīent	7-01223-1	52
P1017T	B2 TURBINE IN	7-01265-801	17
91171P	BGG FUL ORFC BLK IN P	7-01.226-3	41

6.11 FRAGMENTATION SURVEY

- 6.11.1 As part of the activities of the hardware investigation committee a survey was conducted to locate and identify all fragments of the missile blown from the stand area during the explosion. The locations of all fragments discovered was recorded on a map of the area (reproduced on the following page) and each fragment was inspected and identified by Convair and Rocketdyne personnel.
- 6.11.2 The locations of the individual fragments is not considered significant. The majority of the fragments were recovered from the flame deflector wash and the fuel skimming pond after it was drained. The majority of the fragments were found where they were carried by flame deflector water.
- 6.11.3 Exceptions to this are fragments number 4, 6, 7 and 32 which were located where they fell.
- 6.11.4 A list identifying individual fragments shown on the distribution plan is reproduced on page 19.







FINAL ACCIDENT REFORM RUN S2-212-B4-01

6.12 Individual Fragment Identification List

- 1) Instrumentation pickup.
- 2) 3 small steel fragments, heavily carboned on one side.
- 3) Fragment marked 4-1102-75.
- 4) Second Stage Sustainer Turbine wheel
- 5) S cap fitting, marked with orange paint. Does not appear to have come from the explosion.
- 6) Aluminum fragment.
- 7) Strap for retaining boot.
- 8) Two inch piece of drain line
- 9) 3-4 inch fragment, probably from the Sustainer GG exhaust duct manifold.
- 9A) Similar to number 9. Located one foot to the south...
- 10) Cable assembly with a brass identification band stamped J-3067-2.
- 11) Two identification tags and a two inch piece of line marked as follows:

TAG NUMBER ONE: 4600 PSIG

TVA 71230-13

Set at 4600 psig TAG NUMBER TWO:

89-34906-002-13 7-17706-13 CVA - 01 TWO INCH PIECE:

- 12) Part of an Igniter cable
- 13) Another igniter cable.
- 14) A piece of cable with color coded wiring. Does not appear to have come from the explosion.
- 15) A group of parts found together including:
 - a) An igniter cable and a Vernier Igniter clamp marked 9512412-07
 - Six fittings for attaching the boots. These parts appear to have been brought together by flame deflector water action.
- 16) Two small metal fragments
- 17) One of the boits which attaches the second stage turbine wheel to the turbine shaft.
- 18) Fragment



6.12 (Cont'd)

- 19) Turbine wheel blade.
- 20) 2-3 inch fragment
- 21) 2-3 inch fragment
- 21A) Large twisted fragment. 20, 21 & 21A all appear to have come from the Sustainer GG exhaust system.
- 22) Two pieces of tubing, a fitting holding them together, and a small (separate) piece of aluminum. The tubing appears to be part of the Sustainer drain lines.
- 23) A piece of Sustainer "Broomstick" igniter which does not seem to have been exposed to weather and is probably from Run S2-212-B4-O1.
- 24) A fragment and an identification tag marked 7-67742-801 CVA -01
- 25) A one inch piece of tubing.
- 26) A piece of aluminum probably from one of the fittings used to attach the boots.
- 27) A turbine wheel blade.

All parts numbered 28 through 42 were found in the Skimming Pond with the exception of number 32.

- 28) A large piece of the Sustainer GG exhaust.
- 29) A large thicker fragment. Appears to be from the Sustainer GG exhaust manifold.
- 30) Two pieces of Sustainer Thrust Chamber re-inforcing bands.
- 31) Piece of tubing. Probably from one of the Sustainer drain lines.
- 32) Aluminum tag stamped number one.
- 33) Sustainer Turbine Second Stage Inlet Nozzles.
- 34) Eighteen inch section of the Sustainer GG exhaust duct.
- 35) Part of the Sustainer GG exhaust duct manifold.
- 36) The Sustainer Pneumatic Helium Heat Exchanger coils.
- 37) Four pieces of U channel considerably deformed. Probably Sustainer thrust chamber reinforcing bands.
- 38) Three pieces of strap.

-CONFIDENTIAL FINAL ACCIDENT REPORT RUN S2-212-B4-01

6-12 (Cont'd)

- 39) LN2 shroud duct marked 7-87570-BN-01.
- 40) Two pieces of the Sustainer thrust chamber wall tubing.
- 41) A group of fragments from the Sustainer GG exhaust duct and exhaust duct manifold.
- 42) A piece of the fiberglass firewall.

Miscellaneous - A collection of small fragments, fittings, etc., placed in a box marked "Misc. parts Run S2-212-B4-01."

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7.0 CONCLUSIONS

The explosion was caused by damaged seals in the Sustainer Gas Generator LO2 blade valve. These seals were damaged at cutoff during Run 2Ll. LO2 was flowing past the Sustainer Gas Generator blade valve from a time early in Lox tanking. LO2 saturated the residual material in the Sustainer Gas Generator, Sustainer Turbine and the Gas Generator exhaust duct and manifold. The resulting hydrocarbon gels were detonated by the Sustainer Gas Generator igniters firing. The explosion was centered in the Sustainer turbine probably at a point between the first stage turbine wheel and the second stage nozzles. Secondary explosions may have occurred in the exhaust duct and manifold. The cause of the LO2 blade valve seal failure has not been positively determined. It is suspected that the seals were damaged by a minor explosion which occurred between the Sustainer gas generator injection head and the LO2 manifold at cutoff on Run 2Ll. A second and less probable theory is that the seals became misaligned and were damaged by the LO2 blade valve closing.



FINAL ACCIDENT REPORT RUN S2-212-B4-01

8.0 RECOMMENDATIONS AND CORRECTIVE ACTION

- 8.1 It is recommended that Gas Generator purge procedures be reviewed and implemented to ensure adequate purge pressure and duration. During the next test firing of missile 1B it is planned to modify purge procedures. GG purges will be turned on five seconds prior to Vernier engine start and continued for ten minutes after cutoff. Purge source pressure will be increased to ensure adequate purge pressure.
- 8.2 Gas Generator propellant flows and temperature measurements should be checked during propellant tanking and after firing to aid in detecting leaks.
- 8.3 The S2 water and CO₂ fire fighting systems were demonstrated to be adequate in controlling a fire of this nature. It is recommended that these systems be mandatory for all static firings
- 8.4 Closing of pre-valves as a part of emergency fire procedures should be adopted as standard procedure for all static firings. Iocal controls for the Booster and Sustainer pre-valves should be provided.

APPENDIX A

FINAL COUNTDOWN
RUN 52-212-B4-01



PAGE 001	LOCATION OR PANEL					,	FLANE DEFL	FUEL TAKAG	,		רסה כיודער		 ade CHRL	#	
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HYDRAULIC

2000 PSIG 75 PSI XX

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CYC S-2 1-5 RUN- 4 AS RUN COUNTUBL	14 JUL 58	3 PAGE 022	
0054 * CHILLDOWN LGZ SYSTEM FOR TANKING	. It does the second contract the second sec	,	t .
1 - CLOSE RETURN VALVE	The transport of the tr	רסק כיונאר	مياد منتور» بد ا
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7- UPEN PUNP DUTLET VALVE	•••	EOS CHIRL	
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9- CLOSE STORAGE TANK /ELT VEV		LOZ C 173L	
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4- NEPOLT TANK LEVEL _ 20 IN LATERVALSZ	and the state of the second of	Lon
A COUNTY AND A COLUMN AND ADDRESS TO THE ADDRESS AND A	10 PSI NX	PRESS
6056 * LUZ TELKI 1G RECORDENS ON SLUW/CINCUIT		INST CNTAL
0057 - * ACTIVATE PU VALVE CONTROL PROGRAMIER & KEPOKT		
ILL SW OFF		Logia
2- 400 CYCLL SW O'.		Issi
3- 25 VDC 51, 011		INST
4- SIGNAL DC/400 LYCLE SW TO DC	France Common composition of the	INST
5- STEP SW TO CYCLE START	•	IAST
6- CHECK STEPPING SH ROTON SET AT STANT		INST
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SYC 5-2 1-3 RULL GOUITDON	2058 * PERFORM FIGURE GITTE PROGRAMMER		1- CHECN ARMEDISAFE ST TO SAFE	2- ENGINE CUTOFF LOCKOUT SIT O.	3- GINBAL THE DOOSTER SUS & VERNIER	THRUST CHANCERS AT 1 DEG 5 1/2 CPS FOR APPAUX	4- CHECK PRESSUNIZING TIVER SET	FOR 87 SEC	5- CHECK SUS CUTOFF TIMER SET FOR	7 SEC	6- APTER PROGNALICE HAS NECYCLED, ELIC	CUTOFF LOCKOUT S. OFF	0059 * LOTIFY SECURITY-COULTOOLS TINE IS NOW	UD61 * CHECK GINDALING PROGRAM CO. PLETE	COST " CANERAG PUBLIN SA ON LOCATION NIGHT DAY USES	OC62 % OANGON, FECOLOERS TO USE POSITION	COCS & CHECK AND TIMERS NEEDY	1- CHECK LENG TIVES SET FOR 105 JEC	····	21 CHECK SUS ENG TIME? SET MON 189 DEC	TO SO KEEL MOOFK
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2 * 7000	ALL CO.TROLS SATISFACTORY CHECK-REPORT		
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	715241	S PULP SEARINGS-LO2	2116-2	09+	000 DGF		
	P1236T	S GAS GEN DISCANAGE	0117-2	1	14000GF	1	
	P1213T	51 TURDING SEARING	0118-1		750 DGF		
	P1209T	82 TURBILL BEARING	0113-2		750 DGF		,
	P1323T	S TURBINE BEARING	5110-3		750 067		
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	F1125P	B CTL PNEU RES	0111-1	735	765 PIG		, , ,
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APPENDIX B

OBSERVERS VERBATIM
TESTIMONY

RUN S2-212-B4-01

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This decrement contains information effecting the national defense of the United States within the meaning of the Espienage Laws, Title 18, U.S.C., Bestian 793 and 794, the transmission or revolution of which in any manner to an unauthorized person is prohibited by law.

FINAL ACCIDENT REPORT RUN S2-212-B4-01

VISUAL OBSERVER: K. E. Newton, Chief Test Conductor

LOCATION: Right Blockhouse Periscope

 ${\rm LO_2}$ tanking, tank pressurization, vents and Vernier ignition appeared normal. Booster and Sustainer ignition appeared short. Observed a fire and smoke coming out of thrust section and enveloped the Bl area. Firex and ${\rm CO_2}$ came on and fire was immediately extinguished.

S/ K. E. Newton
K. E. Newton

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VISUAL OBSERVER: R. R. MacDougal, S2 Stand Engineer

LOCATION: Middile Blockhouse Periscope

LO₂ tanking, tank pressurization, vents and ignition appeared normal. First noticed puff of fire and smoke apparently concentrated around Bl. The viewing angle could cause smoke around the Sustainer to appear concentrated around Bl.

R. R. MacDougal
R. R. MacDougal



CONFIDENTIAL FINAL ACCIDENT REPORT RUN S2-212-B4-01

VISUAL OBSERVER: E. R. McFadden, Test Conductor

LOCATION: Left Blockhouse Periscope

During ignition stage attention was directed to Sustainer Tachometer speed recorder. An abrupt rise and drop of recorder was noted during ignition. Started for periscope; when fire warning came from tank observer, immediately called for cutoff, CO₂ and firex.

S/ E. R. McFadden
E. R. McFadden



FINAL ACCIDENT REPORT RUN 52-212-B4-01

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VISUAL OBSERVER: R. C. Lynch, Asst. Test Conductor

LOCATION: Blockhouse TV

Was watching test conductor's conscle and two channels of closed loop TV. Vernier ignition appeared reasonably normal as did early ignition stage on main chambers. Mainstage never developed either on TV or on test conductor's console. My first indication of a malfunction was at the end of ignition stage, or where ignition stage should have ended. Hear no explosion but suddenly saw what appeared to be burning fuel falling from the thrust section between the Sustainer engine and Bl on the Quad I side of the missile. Light indications on test conductor's consoles where improper at this time, but I cannot recall to what extent they were wrong.

Depressed Vernier cutoff buttom at first indication of the malfunction and commenced the activation of fire fighting system.

S/ R. C. Lynch R. C. Lynch



FINAL ACCIDENT REPORT. RUN. S2-212-B4-01

VISUAL OBSERVER: C. H. Oliver, Test Engineer

LOCATION: North Tank Observer

V2 ignition appeared normal. Booster and Sustainer ignition start appeared normal. Almost immediately after ignition start observed Vernier cutoff: Ignition stage suddenly appeared as a fire with flames billowing out around the thrust section. Fire seemed concentrated under Bl and Sustainer engine. Called for cutoff. Firex and CO₂ came on and fire was promptly extinguished. CO₂ turned off. Shortly afterwards the fire flared up again. CO₂ was turned on and fire again extinguished. CO₂ was turned off and firex was left on. No further indication of fire. Detanking of LO₂ appeared normal. Fuel leak during attempt to detank fuel could not be seen from north tank due to firex water, LN₂ flush water and heavy vapor.

S/ C. H. Oliver C. H. Oliver



FINAL ACCIDENT REPORT RUN \$2-212-B4-01

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VISUAL OBSERVER: Frank DiPiazza, Test Engineer

LOCATION: South Tank Observer

First sited a fuel rich abnormal Vernier engine ignition and then the appearance of mainstage and an immediate cutoff. Sound of cutoff was present. At that time, I noticed a spreading fire in the area of Vernier engine VI, and immediately I reported fire.

S/ F. DiPiazza F. DiPiazza

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FINAL ACCIDENT REPORT RUN S2-212-B4-01

VISUAL OBSERVER: Dane Allard, Photographer

LOCATION: Photo Tank Observer

₹# #- ~ As the main engines ignited I noticed a burst of flame and smoke which seemed to be concentrated under the Sustainer and Bl engines. The flames and smoke engulfed the lower section of the missile. After the fire was extinguished a second flare-up occurred which was also promptly extinguished.

S/ Dane Allard
Dane Allard

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APPENDIX C

SUMMARY OF DATA PRESENTATION BY MEASUREMENT NUMBER

RUN S2-212-B4-01

NOTE: Appendix C lists all measurements recorded during Run 212 and describes the method employed in analyzing each record. The following abbreviations are used in column headings.

TAB: Tabulated

GRA: Graphical presentation NOT SIG: Not significant NOT REV: Not relavent

APPENDIX -CSUMMARY OF DATA PRESENTATION BY MEASUREMENT NUMBER RUN S2-212-84-01 18 JUNE 58

# U U	DESCRIPTION	REPORT	NOT	NO.	COMMENT
# 25 C		TAB GRA	516	REV	•
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A1264D	MSL TK MOVEMENT X AX	×		₽.	
A1266D	MSL TK MOVEMENT Y AX	×			
41386T	ENG COMP AFT AMB Q1	×			ı
A1387T	ENG COMP AFT AMB Q2	×			
A1388T	ENG COMP AFT AMB Q3	×			
A1389T	ENG COMP AFT AMB 04	*	,	1	
210067	INVERTER PHASE A		×		114 V
E1023V	EXT AC PHASE A		×		104.64 V
E1027V	PROP CONTROL INPUT	×		1	ě
E1028V	MSL SYSTEMS INPUT	×			
F1001P	LO2 TANK HELIUM	×			ı
F1003P	FUEL TANK HELIUM	×	1	_	,
F1005P	B TK HE BTL DISCH	×			
F1011P	LO2 PRES REG DISCH	×			1

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FUEL PRES ORFS DP	LO2 TK HE LN & ORFC	GOZ BO LN @ ELBOW	GO2 BO ELBOW TAP DP	LO2 PRES REG INLET	B CTL HE BRL DISCH	S TK HE BTL DISCH	B CTL PNEU REG	S CTL PNEU REG OUT	S CTL HE BTL DISCH	LO2 PRES ORFC DP	FUEL PRES ORFC IN	FUEL PRES ORFC IN	GO2 BO LN @ ELBOW	LO2 PRES REG IN	BCTL HE BTL DISCH	S TK HE BTL DISCH	B CTL HEAT XGR OUT	S CTL 'HE BTL DISCH	LO2 PRES ORFC IN	AIRBORNE REGS SUP	MSL HYD PUMP DISCH	B1 HYD ACCUMULATOR	S HYD ACCUMULATOR
F1034P	F1065P	F1366P	F1067P	F1114P	F1121P	F1124P	F1125P	F1142P	F1145P	F1147P	F1212P	F10171	F1064T	FIIIST	F1122T	F1123T	Filsot	F1144T	F1146T	F1219T	H1003P	H1033P	H1052P

INVALID DATA

V HYD PUMP DISCH	MSL HYD PUMP DISCH	S HYD PUMP DISCH	V HYD OIL SUPPLY
H1140P	H1001T	H1131F	H1141,T

X	
WATER	
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STRUT	STRUT	STRUT	STRUT
AUX	AUX	AUX	AUX
TOT	TOT	TOT	TOT
L1155S	11156 S	L1157S	L1158S

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SPEED	SPEED	SPEED
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P1055P	P1056P	P1056P	P1059P	P1059P	P1060P	P1060P	P1075P	P1091P	P1092P	P1093P	P1094P	P1100P	P1177P	P1178P	PI181P	P1182P	° P1235P	P1236P	P1280P	P1330P	P1332P	P1337P	P1339P	P1341P	P1344P

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P1350P	P1351P	P1489P	P1007R	Ploobr	P1037R	P1042R	P1043R	P1051R	P1333R	P1334R	P1014T	P1017T	PlolsT	P1020T	P1021T	P1126T	P1127T	P1209T	P1213T	P1323T	P1324T	P1336T

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`×>	PROP ST PRES RELAY	P1135X
××	VERN FUL TK PRES SOL VERN TKS PRES RELAY	P1079X
××	BOOSTER CUTOFF RELAY VERN LOZ TK PRES SOL	P1072X P1078X
< ×	B GG VLV CLSD MSW	P1071X
× >		P1069X
×	BI LOZ VLV CLSD MSW	P1068X
×	B2 LO2 VLV CLSD MSW	P1067X
×	B1 RCC BINARY COUNT B2 RCC BINARY COUNT	P1454W P1455W
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P1223X	P1225X	P1226X	P1227X	P1228X	P1229X	P1230X	P1299X	P1335X	P1347X	P1427X	P1429X	P1438X	P1441X	P1443X	P1444X	P1645X	P446X	P1499X	P1503X	P1510X	P1512X	P1515X	P1516X	P1519X

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P1561X	P1566X	P1568X	P1575X	P1580X	P1581X	P1582X	F1583X	P1586X	P1587X	P1588X	P1591X	P1592X	P1593X	P1594X	P1595X	P1'596X	P1598X

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S1061D	S1062D	S1063D

CAN TEMP
GYRO
S1263T

PROG PITCH SIG	PROG ROLL SIG	BI PCH ACTR FEEDBAK	B2 PCH ACTR FEEDBAK	V1 YAW ACTR FEEDBAK	V2 YAW ACTR FEEDBAK	V2 ROL ACTR FEEDBAK	VI ROL ACTR FEEDBAK	GYRO TEST SIGNAL	BI YAW ACTR FEEDBAK	
S1048V	S1049V	S1107V	S1108V	S1113V	S1114V	S1118V	81119V	S1121V	S1128V	

R FEEDBAK	R FEEDBAK	S PCH ACTR FEEDBAK	FEEDBAK	TEST SIG	TEST SIG
A ACT	# ACTR	ACTR	ACTR	ERVO	SERVO TEST
B1 YAW ACTR	B2 YAW	S PCH	S YAW ACTR	PCH SERVO TEST	YAW SI
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S1235X PROGRAM RUN TIME

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BOOSTER COF DISCRETE	BOOSTER COF PRGR OTP	JETTISON BOOSTER SIG	PRES VERN TKS DISC	PRES V TKS PRGR OTP	SUSTAINER COF DISC	SUS CUTOFF PRGR OTP	PRE-ARM DISCRETE	PRE-ARM PRGR OTP	VERNIER COF DISCRETE	VERNIER COF PRGR OTP	EJECT NOSECONE UMBIL	RELEASE NOSECONE	FIRE RETRO-ROCKETS	WT & THS SYS TANKING	S LUB PUMP BRG	SUS HYD FLOW RATE	S ENG CTL MAN	B ENG CTL MAN	V LO2 TK PRES SOL	V LO2 TK PRES VLV	B1 HYD ACUM
S1236X	S1237X	S1238X	S1239X	S1240X	S1241X	S1242X	S1243X	S1244X	S1245X	S1246X	S1247X	S1248X	S1249X	ST219F	ST206P	STOOIR	ST160T	ST161T	ST162T	ST163T	ST164T

£

ST165T	S HYD ACUM	×		
ST166T	S HYD RES	×	,	1
ST168T	LO2 ST TK PRES SOL	×	•	•
ST169T	B1 LO2 VLV CLOS CTL	×		
ST170T	B2 L02 VLV CLOS CTL	×		1
ST183T	B2 THS CHM Y AX INPD EXT		×	66-85 DEG F
ST184T	BI THS CHM Y AX INBD EXT		×	75-101 DEG
ST185T	B2 THS CHM Y 1145 DEG EXT	×		
ST186T	B1 THS CHM Y 445 DEG EXT		×	75-113 DEG
ST209T	FIRE DETR SKIRT SECT	×		
ST214T	VIBRATRON CASE TEMP	×		,
,			:	
210015	THE GAD TWY BOS		×	
ST152V	A/P 400 CY REF PH A		×	ţ
ST215X	VIBRATRON PRINT READOUT	×		
				1
U1107C	PU SV AMP OUT		×	1
U1021P	LOZ TK HD VIBROTRON		×	
U1022P	FUEL TK HD VIBROTRON		×	
			i	
010910	ERROR RATIO DEMOD OP		×	
U1105V	PU SV COMMAND SIG		×,	1

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APPENDIX D

DETAILED CHRONOLOGICAL HISTORY OF SIGNIFICANT DATA

RUN S2-212-B4-01

DETAILED CHRONOLOGICAL HISTORY
OF SIGNIFICANT DATA
S2-212-84-01 18 JUNE 58

C MEAS DESCRIPTION EVENT	-2 P1336T S GAS GEN DISCH DEC FROM 117 DEG F TO PEG NEG	-2 F1003P FUEL TANK HELIUM INC FROM SEG II TO III /55.3 PSIG/	-2 PI337P SGG LOZ INJ MAN INC FROM 1.26 PSIG TO 16.70 PSIG		-1 E1027V PROP CONTROL INPUT ON INT SWGVER ATTEMPT	-2 E1028V MSL SYSTEMS INPUT INC FROM 27.7 TO 34V ON INT SWOVER ATMP	-2 E1028V HSL SYSTEMS INPUT BACK TO EXT AFTER 19 SEC	-1 E1027V PROP CONTROL INPUT INC FOR 7 SEC ON 2ND INT SWOVER ATTEMPT	-2 E1028V MSL SYSTEM INPUT 2ND SWOVER ATTEMPT 34V FOR T SEC	-1 E1027V PROP CONTROL INPUT INC FOR 16 SEC ON BRD INT SMOVER	-1 E102TV PROP CONTROL INPUT ATTEMPT	-2. E1028V MSL SYSTEMS INPUT 3RD SWOVER ATTEMPT 34V FOR 16 SEC	-1 PIO03P BZ LOZ PUMP IN OSCILLATES & 8 CPS FOR 345 SEC	-1 PIOOIP BI LOZ PUMP IN OSCILLATES FOR 1.5 SEC . 4 CPS	-3 PIOS6P S LOZ PUMP INLET OSCILLATES FOR 1 SEC . CPS	-3 FIGILP LOZ PRES REG DISCH INC FROM 25 TO 26.5 PSIG	-2 FIGO3P FUEL TANK HELIUM INC FROM 55.5 TO 57.8 PSIG IN 27.7 SEC	-9 P1056P S LO2 PUMP INLET OSCILLATES FOR .6 SEC # 11 CPS	を申請者 雅一 中華 日本 日本 日本 日本 日本 日本 日本 日本 日本 日本 日本 日本 日本
MEAS	P1336T	F1003P	P1337P	E1027V	E1027V	E1028V	E1028V	E1027V	E1028V	E1027V	E1027V	E1028V	P1003P	PlooiP	P1056P	F1011P	F1003P	P1056P	
REC	117-2	119-2	208-2	221-1	221-1	221-2	221-2	221-1	221-2	221-1	221-1	221-2	122-1	123-1	123-3	121-3	119-2	123-3	
TIME	-467.13	-299.83	-214.13	-149,13	-149.13	-149.13	-149.12	-129.13	-129,13	-105.63	-105.63	-105,63	-38.13	-38.03	-37.93	-31.36	-30.89	-30.43	

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STEADY 3130 PSIG	STEADY 3200 PSIG	STEADY 60 DEG F	STEADY MINUS 175 DEG F	DEC FROM MINUS 28% TO MINUS 291 DEF F	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	DEACTIVATE	TRANSIENT SOB TO 498 TO 514 PSIG	INC FROM AMB /MINUS 14/ TO 915 PSIG	DEC 533 PSIG TO 524 PSIG	INC FROM AND CHINUS & PSIG/ TO 527 PSIG	TRANSIERT 529 TO 479 TO 529 PSIG	INC FROM AMB /62 PSIG/ TO \$24 PSIG	INC FROM AMB/67 PSIG/TO SIE PSIG	TANK PRESSURIZES	INC FROM AMB/48 PSIG/ TO 495 PSIG	INC FROM AMB /32 PSIG/ TO SIP PSIG	INC FROM AMB /32 PSIG/ TO \$20 PSIG	INC FROM 16. TO PSIG TO 35.20 PSIG	INC FROM AMB /167 PSIG/ TO 956 PSIG	ACTIVATE	ACTIVATE
B TK HE BTL DISCH	B CTL HE BTL DISCH	FUEL PRES ORFC IN	B CTL HE BTL DISCH	LOZ AT BREAKWAY VLV	TCC VERN ENG STR SW	VERN LOZ TK PRES SOL	VERN FUL TK PRES SOL	VERN TKS PRES RELAY	PROP S T PRES RELAY	VERN LOZ VENT CONT	B LOZ START TANK REG	VERNIER LOZ TANK	VERN FUEL TANK REG OUT	VERNIER FUEL TANK	VERN, LOZ TK REG OUT	VI FUEL INLET	VZ FUÉL INLET	G FUEL START TANK	B GAS GEN LOZ VLV IN	VZ LOZ INLET	VI LOZ INLET	SGG LOZ INJ MAR	SGG FUEL VLV INLET	STRT TKS PRESS TIMER	VERN SQUIBS, FIRING
F1005P	F1121P	FIOITT	F1122T	P1021T	PII61X	P1078X	PIOTOX	X9601d	PII35X	P1427X	P1177P	P1030P	P1236P	P1627P	P1235P	P1049P	P1050P	P1075P	P1489P	P1048P	P1047P	P1337P	P1280P	P1568X	P1516X
217-2	217-1	CEC	222-1	123-2	52	27	56	25	Ř	24	113-3	109-1	110-2	110-1	109-2	209-3	210-1	1,10-3	109-3	208-2	209-1	208-2	208-3	30	28
-25.00	-25.00	-25.00	-25.00	-17 _e 15	-14.24	-14.23	-14.23	-14.23	-14.23	-14.23	-16.22	-14.21	-14.18	-14.17	-14.17	-14.13	-14.13	-14-13	-14.11	-13.99	-13.96	-13.93	-13.84	-12.18	• 60

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STEADY AT 737 PSIG	ACTIVATE	ACTIVATE	ACTIVATE	TRANSIENT - 519 TO 366 TO 502 PSIG	TRANSIENT SIG TO 271 TO 450 PSIG	BEGAN OSCILLATION FOR . SEC	DEC FROM SIG PSIG TO SIG PSIG	TRANSIENT 525 TO 518 TO 528 PSIG	INC FROM AMB /B PSIG/ TO 188 PSIG		DEC FROM MINUS .8 PSIG TO PEG NEG	GSCILLATES 4 CPS FOR .6 SEC	INC FROM 16-1 TO 17-0 PSIG	INC FROM 53.6 TO 54.4 PSIG	INC FROM ANB /17 PSIG/ TO 32.2 PSIG	ACTIVATE	ACTIVATE	INC FROM 25 TO 28 PSIG	TRANSIENT 524 TO 290 TO 459 PSIG	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE
S CTL PNEU REG OUT	VERN ENG LOKIN RELAY	VERN PV OPEN CTL	PRES V TKS PRGR OTP	V2 LO2 INLET	V2 FUEL INLET	VI LOZ INLET	VERNIER LOZ TANK	VERN LOZ TK REG OUT	VI THRUST CHAMBER	V2 THRUST CHAMBER	BZ FUEL PUMP INLET	V2 THRUST CHAMBER	FUEL PRES ORFC DP	LO2 PRES ORFC DP	S LUBE PUMP GEAR	TCC VERN COMPLETE LT	BES FUEL INJ PRG SOL	LOZ TK HE LN & ORFC	VI FUEL INCET	BI LOZ V CLOS CTL	B2 LOZ V CLOS CTL	B LO2 V OPEN CTL SOL	SUSTAINER HSV SOL B	SUSTAINER HSV SOL A	S IGN FUEL V OPEN CTL
F1142P	P1165X	P1167X	\$1240X	P1048P	PIOSOP	P1047P	P1030P	P1235P	P1028P	P1029P	P1004P	P1029P	F1034P	F1147P	P1341P	PISIOX	P1166X	F1065P	P1049P	P1149X	P1512X	P1139X	P1196X	P1197X	Pl586X
113-1	33	32	191	209-2	210-1	209-1	109-1	109-2	219-1	219-2	112-2	219-2	CEC-	CEC-	218-3	39	36	CEC-	209-3	113	112	4.5	19	74	99
٠ 9	•63	*9*	•65	•71	•71	•76	•79	. 83	1.03	1.03	1.06	1.27	1.47	1.47	1.47	1.56	1,57	1.67	1.73	1.81	1.81	1,82	1.82	1.82	1.82

THE TOTAL OF

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1.87	108-3	P15290	S MAIN LOZ VALVE	STARTED OPEN FROM O DEG
1.58	123-3	P1056P	S LOZ PUMP INLET	TRANSIENT 46 TO 39 TO 42 PSIG
1.89	221-1	E1027V	PROP CONTROL INPUT	DEC .5 V
1.89	89	X66114	S LOZ HSV CLOSED MSW	DEACTIVATE
1991	84	P1067X	BZ LOZ VLY CLSD HSW	DEACTIVATE
1.93	214-1	H1052P	S HYD ACCUMULATOR	DEC FROM 1640 TO 1590 PSIG
1.93	208-3	P1280P	SGG FUEL VLV INLET	TRANSIENT 956 TO 868 TO 941 PSIG
1.94	123-1	PloolP	BI LOZ PUMP IN	TRANSIENT 51 TO 42 TO 49 PSIG
1.95	110-3	P1075P	G FUEL START TANK	DEC FROM BO4 PSIG / IGN FLOW/
1.95	46	P1068X	BI LOZ VLV CLSD MSW	DEACTIVATE
1.99	216-1	F1145P	S CTL HE BTL DISCH	STEADY AT 3116 PSIG
1.99	122-1	P1003P	B2 LOZ PUMP IN	TRANSIENT 54 TO 42 TO 52 PSIG
2.01	117-3	£1006P	S THRUST CHAMBER	INC FROM AMB
2,01	64	P1169X	B2 LO2 YLY OPEN MSW	ACTIVATE
2.12	110-3	Plo75P	G FUEL START TANK	SURGE TO 941 PSIG
2.17	47	PIITOX	BI LOZ VLV OPEN MSW	ACTIVATE
2.22	69	P1198X	S LOZ HSV OPEN MSW	ACTIVATE
2.27	113-1	F1142P	S CTL PNEU REG OUT	TRANS 742 TO 640 TO 825 TO 633 TO 767
2.27	113-1	F1142P	S CTL PNEU REG OUT	TO 745 PSIG
2.30	119-2	P1339P	S GAS GEN DISCH	TRANSIERT O TO 87 TO 27 PSIG
2.30	50	P1142X	TCC IGN COMPLETE LT	ACTIVATE
2,31	216-2	F1124P	S TK HE BTL DISCH	STEADY AT 1650 PSIG
2,31	111-1	F1125P	B CTL PNEU REG	STEADY AT 749 PSIG
2.31	CEC	P1351P	S LOZ INJ MANIFOLD	BEGAN OSCILLATION FOR .OT SEC
2.31	109-3	P1489P	B GAS GEN LOZ VLV IN	INC FROM 495 PSIG TO 527 PSIG
2.32	CEC	P1055P	S FUEL PUMP INLET	DEC FROM 64.4 PSIG TO 27 PSIG

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2.32	208-2	P1337P	SGG LOZ INJ MAN	TRANSLIFUT AS TO TO SEE OF SE THE TANKENTERS
2,33	CEC+	F1034P	FUEL PRES ORFG DP	TRACE BECOMES FEDATIC NOTES
2,33	CEC-	F1065P	LOZ TK HE LN @ ORFC	TRACE BECOMES FEDDATIC NOTER
2.33	CEC-	F1147P	LO2 PRES ORFC DP	TRACE SECONS AND ALLES
2,33	CEC	F1017T	FUEL PRES ORFC IN	INC FULL SCALE
2.33	109-1	P1030P	VERNIER LOZ TANK	DEC FROM 523 PSIG TO A10 BATG
2+33	CEC	P1100P	BGG COMBUSTION CHM	TRANSIENT OFF SCALE
2.33	113-3		B LOZ START TANK REG	DEC TO 0 PSIG
2.33	208-3		SGG FUEL VLV INLET	DROP FROM 941 TO HINIS 24 pers
2,33	CEC		S FUEL INJ MANIFOLD	TRANSIENT PEG TO PEG
2,33	CEC		S LOZ INJ MANIFOLD	TRANSLENT PEG TO PFG
2,93	123-2		LOZ AT BREAKWAY VLY	INC TO PEG POS FROM MINUS 287.4 DEG B
2.33	en en		BGG VLV CLSD MSW	DEAGTSVATE
2,33	11		ETP PREP COMPLETE LT	DEACTIVATE
2•34	217-2		B TK HE BTL DISCH	DROP FROM 2800 TO 0 PS1G
2.34	222-1		B CTL HE BTL DISCH	DEC FROM MINUS 175 TO MINUS 108 DEG #
2•34	114-2		ATRBORNE REGS SUP	INC FROM 54 DEG F TO PEG POS
2•34	A4-5		S NAA RCC ACCEL	TRANSIENT TO APPROX 66.5 G
2.34	AM-8		BI NAA RCC ACCEL	TRANSIENT TO APPROX 51 G
2.34	218-1		BI LUBE OIL MAN	TRANS AMB /5.4 PSIG/ TO MINUS 2.8 TO
2.34	218-1		BI LUBE OIL MAN	AAB
2+34	218-2		B2 LUBE OIL MAN	6 PSIG TRANSIENT
2.34	123-3		5 LO2 PUMP INLET	USCILLATES FOR 2.6 SEC . 10 CBS
2034	208-1	Раззор	S FUEL PUMP DISCH	TRANSIENT OF TO MINUS 2 TO SOA BREE
2.34	CEC	P1454W	BI RCC SINARY COUNT	Delta de la companya
2•34	55	P1069X	BZ FUEL VLV CLSD MSW	DEACTIVATE

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2.34 112 2.34 403-1 2.34 403-5 2.35 121-2 2.35 119-2 2.35 119-2 2.35 119-3 2.35 119-3 2.35 119-3 2.35 119-3	P1143X P1503X P1512X P1568X S12107V S1217V F1001P F1003P F1114P P1332P P1070X	B GAS GEN IGN LINK GFST VENT CTL B2 LO2 V CLOS CTL STRT TKS PRESS TIMER B1 PCH ACTR FEEDBAK S PCH ACTR FEEDBAK S YAW ACTR FEEDBAK LO2 TANK HELIUM FUEL TANK HELIUM LO2 PRES REG INLET S LO2 PUMP DISCH B1 FUEL VLV CLSD MSW BGG VLV CLOSED MSW B1 LO2 V CLOS CTL	DEACTIVATE DEACTIVATE DEACTIVATE DEACTIVATE DEACTIVATE DEACTIVATE TRANSIENT .5 DEG DN FOR .1 SEC TRANSIENT .25 DEG DN FOR .16 SEC TRANSIENT .5 DEG VAW RT FOR .03 SEC OSCILLATES 23.1 TO 20.7 PSIG OSC 48.2 TO 40.3 PSIG FOR 1.5 SEC DEC FROM 3020 TO 0 PSIG TRANSIENT 44 TO MINUS 8 TO 67 PSIG DEACTIVATE DEACTIVATE
49 22 221~1 111~2 115~3 31 32 47	P1169X P1503X E1027V P1026P P1165X P1167X P1170X	B2 LO2 VLV OPEN MSW GFST VENT CTL PROP CONTROL INPUT B LO2 REG REF B1 THRUST CHAMBER VERN ENG LOKIN RELAY VERN PV OPEN CTL B1 LO2 VLV OPEN MSW MSL SYSTEMS INPUT	DEACTIVATE ACTIVATE DEC TO PEG NEG DEC FROM STEADY 596.3 PSIG TO 530.4 PSI ANB TO 54 PSIG THEN PEGS MINUS DEACTIVATE DEACTIVATE DEACTIVATE TRANSIENT OF .6 V

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2.37	121-3	FIOIIP	LOZ PRES REG DISCR	2701 07 03 123 1202
2.37	216-2	F1124P	S TK HE BTL DISCH	TRANS 3100 TO 2530 TO 3330 TO 2475 TO
2.37	216-2	F1124P	S TK HE BTL DISCH	zeso psig
2.37	108-3	P1529D	S MAIN LOZ VALVE	REACHED MAX POS 86.77 DEG
2.37	129-1	P1001P	61 LOZ PUMP IN	OSCILLATES FOR 1.08 SEC @ 4.8 CPS
2.37	110-1	P1027P	VERNIER FUEL TANK	TRANSIENT 527 PSIG TO 507 PSIG
2037	109-2	P1235P	VERN LOZ TK REG OUT	TRANSIENT 528 TO 429 TO 661 PSIG
2.37	109-3	P1489P	B GAS GEN LOZ VLV IN	DEC TO AMB /48 PSIG/
2,37	M	P1445X	B FUEL PRE VLV OPEN	DEACTIVATE
2.38	115-2	P1059P	B2 THRUST CHAMBER	DEC FROM AMB TO PEG MINUS
2.38	110-2	P1236P	VERN FUEL TANK REG OUT	TRANSIENT \$23 TO 427 TO 554 TO 495 PSIG
2.38	220-2	P1014T	ENGINE COMP AMB	TRANSIENT 45.5 TO 42.5 TO 69.0 DEG F
2.38	117-2	P1336T	S GAS GEN DISCH	TRANSIENT PEG NEG TO 390 TO 124 BEG F
2.38	131	\$1240X	PRESS V TKS PRGR OFP	DEACTIVATE
2.39	69	P1198X	S LOZ HSV OPEN MSW	DEACTIVATE
2.40	222-1	F1122T	B CTL HE BTL DISCH	INC FROM MINUS 193 DEG # TO PEG POS
2.40	222-3	F1130T	B CTL HEAT XGR OUT	INC FROM 82 DEG F TO PEG POS
2.41	122-1	P1003P	BZ LOZ PUMP IN	OSCILLATES & 5 CPS FOR 1+2 SEC
2.41	113-2	P1344P	S LO2 REG REF	OSC 165 FROM 789 PSIG FOR 1.7 SEC
2.41	116-3	P1324T	S PUMP BEARINGS-LO2	DEC FROM 182.5 TO 177 DEG F
2.43	217-1	F1121P	B CTL HE BTL DISCH	DEC FROM 3200 TO 0 PSIG
2.44	213-1	H1140P	V HYD PUMP DISCH	600 PSIG DIP TRANSIENT
2.47	115-2	P1059P	82 THRUST CHAMBER	INC TO 32.80 PSIG
2.48	219-2	P1029P	VZ THRUST CHAMBER	DEC FROM 233 PSIG TO AMB /1 PSIG/
2.48	209-1	P1047P	VI LOZ INLET	BEGAN OSCILLATION FOR .42 SEC
2-48	2002	P1048P	V2 LO2 INLET	TRANSVENT - 466 TO SAS TO SAS PAIG

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COMMERCENCY OF THE COURT OF METERS SECTION AND SECTION OF THE COURT OF

219-1 P1028P V1 THRUST CHAMBER 210-1 P1050P V2 FUEL INLET 209-3 P1049P V1 FUEL INLET 220-2 P1014T ENGINE COMP AMB 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT X AX 117-2 P1396T S CTL HE BTL D1SCH 216-1 F1145P S CTL HE BTL D1SCH 216-1 F1145P S CTL HE BTL D1SCH 109-2 P1396T S GAS GEN D1SCH 1199-2 P1295P VERN LOZ TANK 109-2 P1295P S HYD ACCUNULATOR 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1396T S GAS GEN D1SCH 115-2 A1264D MSL TK MOVEMENT X AX 107-2 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LOZ PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP D1SCH 220-2 P1014T ENGINE COMP AMB	2.50	108-1	P1030P	VERNIER LOZ TANK	INC FROM 410 PSIG TO 668 PSIG
210-1 P1050P V2 FUEL INLET 209-3 P1049P V1 FUEL INLET 220-2 P1004P B2 FUEL PUMP INLET 220-2 P1014T ENGINE COMP AMB 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 216-1 F1145P S CTL HE BTL DISCH 216-1 F1145P S CTL HE BTL DISCH 109-2 P1235P VERN LOZ TAMK 109-2 P1235P VERN LOZ TAMK 109-2 P1235P VERN LOZ TAMK 109-3 P1529D S MAIN LOZ VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 A1264D MSL TK MOVEMENT Y AX 107-2 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LOZ PRES REG IN 110-2 P1236P VERN FUEL TAMK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2°51	219-1	P1028P	V1 THRUST CHAMBER	DEC FROM 220 PSIG TO AMB /8 PSIG/
209-3 P1049P VI FUEL INLET 220-2 P1004P B2 FUEL PUMP INLET 220-2 P1014T ENGINE COMP AMB 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1264D MSL TK MOVEMENT Y AX 216-1 F1145P S CTL HE BTL DISCH 216-1 F1145P S CTL HE BTL DISCH 117-2 P1336T S GAS GEN DISCH 109-2 P1235P VERN LOZ TANK 109-3 P1529D S HYD ACCUNLATOR 115-3 P1060P B1 THRUST CHAMBER 115-4 P1059P B2 THRUST CHAMBER 115-5 P1059P B2 THRUST CHAMBER 117-2 P1336T S GAS GEN DISCH 117-2 P1336T S GAS GEN DISCH 117-3 P1059P B4C THRUST CHAMBER 117-4 P1336T S GAS GEN DISCH 118-5 P1059P B4C TK MOVEMENT Y AX 110-2 P1236P VERN FUEL TANK REG OUT 200-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.52	210-1	P1050P	V2 FUEL INLET	TRANSIENT 450 TO 545 TO 514 PSIG
122-2 P1004P B2 FUEL PUMP INLET 220-2 A1264D MSL TK MOVEMENT X AX 107-3 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 216-1 F1145P S CTL HE BTL DISCH 216-1 F1145P S CTL HE BTL DISCH 117-2 P1336T S GAS GEN DISCH 1109-2 P1235P VERN LOZ TK REG OUT 214-1 H1052P S HYD ACCUNLATOR 1108-3 P1529D S HYD ACCUNLATOR 1115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1059P B2 THRUST CHAMBER 117-2 P1059P B2 THRUST CHAMBER 117-2 P1059P B2 THRUST CHAMBER 117-2 A1264D MSL TK MOVEMENT Y AX 217-3 A1264D WSL TK MOVEMENT Y AX 217-3 F1115T LOZ PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2,53	209-3	P1049P	VI FUEL INLET	TRANSIENT 453 TO 560 TO 522 PSIG
220-2 A1264D A5264D 57	122-2	P1004P	82 FUEL PUMP INLET	TRANSIENT - PEGS POS TO NEG	
107~2 A1264D MSL TK MOVEMENT X AX 107~3 A1266D MSL TK MOVEMENT Y AX 216~1 F1145P S CTL HE BTL DISCH 68 P1199X S LOZ HSV CLOSED HSW 117~2 P1336T S GAS GEN DISCH 109~2 P1235P VERN LOZ TANK 109~2 P1235P VERN LOZ TANK 108~3 P1659P S HYD ACCUNULATOR 115~3 P1660P BI THRUST CHAMBER 115~2 P1356T S GAS GEN DISCH 117~2 P1356T S GAS GEN DISCH 117~2 P1259D S MAIN LOZ VALVE 115~2 P1059P BGG COMBUSTION CHM 115~2 P1256D MSL TK MOVEMENT X AX 107~3 A1266D MSL TK MOVEMENT Y AX 217~3 F1115T LOZ PRES REG IN 110~2 P1236P VERN FUEL TANK REG OUT 208~1 P1330P S FUEL PUMP DISCH 220~2 P1014T ENGINE COMP AMB	2.63	220-2	Ploist		TRANSIENT 69.0 TO 60.5 TO 107.0 DEG F
107~3 A1266D MSL TK MOVEMENT Y AX 216~1 F1145P S CTL HE BTL DISCH 68 P1199X S LO2 HSV CLOSED MSW 117~2 P1336T S GAS GEN DISCH 109~1 P1030P VERN IER LO2 TANK 109~2 P1235P VERN LO2 TK REG OUT 214~1 H1052P S HYD ACCUNULATOR 115~3 P1060P BI THRUST CHAMBER 115~2 P136T S GAS GEN DISCH 115~2 P136T S GAS GEN DISCH 115~2 P136F S GAS GEN DISCH 115~2 P136T S GAS GEN DISCH 115~2 P136F WSL TK MOVEMENT X AX 107~2 A1264D MSL TK MOVEMENT Y AX 217~3 F1115T LO2 PRES REG IN 110~2 P1330P S FUEL TANK REG OUT 208~1 P1330P S FUEL PUMP DISCH 220~2 P1014T ENGINE COMP AMB	2.65	107-2	A1264D		STEADY AT .O25 INCHES
216-1 F1145P S CTL HE BTL DISCH 216-1 F1145P S CTL HE BTL DISCH 68 P1199X S LO2 HSV CLOSED HSW 117-2 P1336T S GAS GEN DISCH 109-1 P1030P VERN ier Lo2 TANK 109-2 P1235P VERN LO2 TK REG OUT 214-1 H1052P S HYD ACCUNULATOR 108-3 P1529D S NAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.65	107-3	A1266D	MSL TK MOVEHENT Y AX	STEADY MINUS .OS INCHES
216-1 F1145P S CTL HE BTL DISCH 68 P1199X S LO2 HSV CLOSED HSW 117-2 P1336T S GAS GEN DISCH 109-1 P1030P VERN LO2 TAMK 109-2 P1235P VERN LO2 TK REG OUT 214-1 H1052P S HYD ACCUNLATOR 116-3 P1529D S MAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER 117-2 P1336T S GAS GEN DISCH 115-2 P1336T S GAS GEN DISCH 115-2 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TAMK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.65	216-1	F1145P	S CTL HE BTL DISCH	TRANSIENT 3079 TO 2391 TO 3288 TO 2257
68 P1199X S LO2 HSV CLOSED MSW 117-2 P1336T S GAS GEN DISCH 109-1 P1030P VERNIER LO2 TANK 109-2 P1235P VERN LO2 TK REG OUT 214-1 H1052P S HYD ACCUNULATOR 108-3 P1529D S MAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER 117-2 P1336T S GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT Y AX 107-3 A1266D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 116-2 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2965	216-1	F1145P	S CTL HE BTL DISCH	TO 265% PSIG
117-2 P1336T S GAS GEN DISCH 109-1 P1030P VERNIER LOZ TAMK 109-2 P1235P VERN LOZ TK REG OUT 214-1 H1052P S HYD ACCUMULATOR 108-3 P1529C S MAIN LOZ VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 117-2 A1264D MSL TK MOVEMENT X AX 110-2 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LOZ PRES REG IN 110-2 P1236P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	59*2	89	P1199X	S LOZ HSY CLOSED MSW	ACTIVATE
109-1 P1030P VERNIER LOZ TANK 109-2 P1235P VERN LOZ TK REG OUT 214-1 H1052P S HYD ACCUMULATOR 108-3 P1529D S MAIN LOZ VALVE 115-3 P1060P BI THRUST CHAMBER 117-2 P1100P BGG COMBUSTION CHM 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT X AX 110-2 A1264D MSL TK MOVEMENT Y AX 217-3 F11157 LOZ PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.68	117-2	Plaser	S GAS GEN DISCH	
109-2 P1235P VERN LO2 TK REG OUT 214-1 H1052P S HYD ACCUNULATOR 108-3 P1529D S NAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-3 A1264D MSL TK MOVEMENT X AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.74	109-1	P1030P	VERNIER LOZ TANK	DEC FROM 683 PSIG TO 410 PSIG
214-1 H1052P S HYD ACCUNULATOR 108-3 P1529D S NAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.77	109-2	P1235P	VERN LOZ TK REG OUT	TRANSIENT 661 TO 458 TO 809 PSIG
108-3 P1529D S MAIN LO2 VALVE 115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1264D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	78.2	214-1	H1052P	S HYD ACCUMULATOR	
115-3 P1060P B1 THRUST CHAMBER CEC P1100P BGG COMBUSTION CHM 117-2 P1336T S GAS GEN DISCH 115-2 A1264D MSL TK MOVEMENT X AX 107-3 A1264D MSL TK MOVEMENT X AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	18.5	108-3	P1529D	S MAIN LOZ VALVE	CLOSING - 1.40 DEG
CEC P1100P BGG COMBUSTION CHM 117-2 P1336T \$ GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P \$ FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	2.96	115-3	P1060P	BI THRUST CHAMBER	DEC FRUM 302.8 PSIG /MAK/ TO PEG MINUS
117-2 P1336T S GAS GEN DISCH 115-2 P1059P B2 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 217-3 F1115T LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	16*2	CEC	P1100P	BGG COMBUSTION CHM	TRACE RETURNS TO AMB
115-2 P1059P 32 THRUST CHAMBER 107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 217-3 F11157 LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	\$692	117-2	P1336T	S GAS GEN DISCH	DEC FROM 140 DEG F TO PEG NEG
107-2 A1264D MSL TK MOVEMENT X AX 107-3 A1266D MSL TK MOVEMENT Y AX 217-3 FILLST LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	3.01	115-2	P1059P	32 THRUST CHAMBER	DEC FROM 176.0 PSIG TO PEG MINUS
107-3 A1266D MSL TK MOVEMENT Y AX 217-3 FILLST LO2 PRES REG IN 110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	3.27	107-2	A1264D	MSL TK MOVEMENT X AX	INC TO .125 INCHES
217-3 FILLST LOZ PRES REG IN 110-2 PI236P VERN FUEL TANK REG OUT 208-1 PI330P S FUEL PUMP DISCH 220-2 PI014T ENGINE COMP AMB	1.27	107~3	A1266D	MSL TK MOVEMENT Y AX	INC TO MINUS .025 INCHES
110-2 P1236P VERN FUEL TANK REG OUT 208-1 P1330P S FUEL PUMP DISCH 220-2 P1014T ENGINE COMP AMB	8.30	217-3	FILLST	LO2 PRES REG IN	INC FROM 80 DEG F TO PEG NEG
208-1 Plagop s FUEL PUMP DISCH 220-2 Ploi47 ENGINE COMP AMB	3.30	110-2	P1236P	VERN FUEL TANK REG OUT	TRANSIENT SIG TO 426 TO 474 PSIG
220-2 PIO147 ENGINE COMP AMB	1.31	208-1	P1330P	S FUEL PUMP DISCH	TRANSIENT 95 PSIG TO 39 PSIG TO 66 PSIG
	3.31	220-2	P10147		TRANSIENT 107.0 TO 104.3 TO PLUS PEG

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ACTIVATE	MAX DEFL - 6 PSIG	FULL CLOSED	DEC TO . B PSIG	STABLE AT 28.3 V	ACTIVATE	ACTIVATE	DEC FROM 936 PSIG TO AMB /MINUS 14 PSIG	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	ACTIVATE	INC FROM PEG NEG TO MINUS 3+5 PSIG	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	ACTIVANE	DEC FROM 475 TO AMB /MINUS 6 PSIG/	. DEACTIVATE	DEACTIVATE	DEACTIVATE		DEACTIVATE	
B IGN DETR DELAY-PU	S THRUST CHAMBER	S MAIN LOZ VALVE	B CTL PNEU REG	HSL SYSTEMS INPUT	VERN COF REL LOCKIN	DC GND PWR FAIL COF	VERNIER LOZ TANK	S COF RELAY LOCKIN	S LOZ REG VENT V CTL	VERNIER ENG COF	SUS CUTOFF PRGR OTP	VERNIER COF PRGR OTP	82 FUEL PUMP INLET	VERN COF REL LOCKIN	DC GRND PWR FAIL COF	s LO2 REG VENT V CTL	VERNIER ENG COF	BOOSTER COF PRGR OTP	VERNIER FUEL TANK	VERN LOZ TK PRES SOL	VERN FUL TK PRES SOL	PROP S T PRES RELAY		ETP PREP COMPLETE LT	PRE IGN
P1299X	P1006P	P15290	F1125P	E1028V	P1077X	P1566X	P1030P	P1347X	P1582X	P1598X	S1242X	S1246X	P1004P	P1077X	P1566X	P1582X	P1598X	\$1237X	P1027P	PIOTEX	P1079X	P1135X		P1137X	P1137X P1342X
24	117~3	108-3	111-1	221-2	<i>w</i>	93	108-1	0	102	101	133	137	122-2	86	80	102	101	126	110-1	27	26	23	•	~	- O
3.37	3.40	3.42	3.79	3.87	5.08	5.08	5.09	5.09	5.09	8000	5.09	5.09	5.10	5.10	5.10	5.10	5+10	5.10	5.11	5.11	5011	5.11	•	7110	5.11 5.11

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/ATE	ATE	ATE	ATE	ATE	Ħ	ATE	ATE TO THE TENT OF	ATE	ATE	ATE	ATE	ATE	TRANSIENT 488 TO 905 TO 483 PSIG	DEC FROM 568 TO AMB /32 PSIG/	DEC FROM 514 PSIG TO AMB /67 PSIG/	IM %22 PSIG TO AMB /82 PSIG/	NA 549 PSIG TO AMB /32 PSIG/	NIS	INC TO MINUS .020 INCHES	TRANS 2750 TO 3000 TO 2640 TO 2800 PSIG	TRANSIENT 737 TO 798 TO 697 TO 736 PSIG	TRANSLENT 2473 TO 2770 TO 2943 TO	316	OSC 59.0 TO 52.5 PSIG FOR .5 SEC	TRANSIENT 483 TO 550 TO 453 TO 476 PSIG
DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	ACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	TRANSIE	DEC FRC	DEC FRC	DEC FROM \$22	DEC FROM 549	TANK VENTS	INC TO	TRANS	TRANSIE	TRANSIE	2484 PSIG	86° 380°	Trans I e
BES FUEL INJ PRG SOL	SUSTAINER HSV SOL B	SUSTAINER HSV SOL A	B 16N DETR DELAY-PU	S COF RELAY LOCKIN	VERN LOZ VENT CONT	GFST VENT CTL	TCC VERN COMPLETE LT	VERN SQUIBS FIRING	S IGN FUEL V OPN CTL	SUS CUTOFF PRGR OTP	VERNIER COF PRGR OIP	VERN TKS PRES RELAY	VERN LOZ TK REG OUT	V2 LO2 INLET	V2 FUEL INLET	VI FUEL INLET	VI LOZ INLET	G FUEL START TANK	HSL TK MOVEMENT Y AX	S TK HE BTL DISCH	S CTL PNEU REG OUT	S CTL HE BTL DISCH	S CTL HE BTL DISCH	FUEL TANK HELIUM	VERN LOZ TK REG OUT
P1166X	P1196X	P1197X	P1299X	P1347X	P1427X	PISO3X	PISIOX	P1516X	P1586X	S1242X	S1246X	P1096X	P1235B	P1048P	PAOSOP	P1049P	P1047P	P1075P	A1266D	F1124P	F1142P	F11450	F1145P	F1003P	P1235p
36	47	14	42	0.0	24	22	90	88	99	66 m	137	2 3	109-2	209-2	210-1	209-3	209-1	110-3	107-3	216-2	113-1	216-1	216-1	119-2	109-2
5.11	5,11	5,11	5.11	5.11	5,11	5.43	5.11	5.11	5.11	5.11	5,11	5.12	5.13	5.17	5.17	5.19	5.20	5.21	7967	7.87	7.87	7.87	7.87	7.89	7.92

123-1 P1001P B1 LO2 PUMP IN 220-2 P1014T ENGINE COMP AMB 107-2 A1264D MSL TK MOVEMENT X AX 122-2 P1004P B2 FUEL PUMP INLET 208-3 P1280P SGG FUEL VLV INLET 107-3 A1266D MSL TK MOVEMENT Y AX 86 P1588X S T6N OVERSPEED TRIP	12.093 13.55 14.02 14.02 17.03 17.03 17.03 17.03 17.03 17.03 17.03 17.03 17.03 17.03 17.03	110-2 119-3 214-1 121-2 121-2 113-2 216-1 216-3 117-3 122-2 213-3 122-2 213-3	P1236P P1332P H1052P F1001P F1011P P1344P P1344P P1065P P1065P P1581X P1055P P1580X P1056P P1056P	S LOZ PUMP DISCH S LOZ PUMP DISCH LOZ TANK HELLUM LOZ PRES REG DISCH S LOZ REG REF S CTL HE BTL DISCH S LUBE PUMP GEAR S THRUST CHAMBER BZ FUEL PUMP INLET V HYD GIL SUPPLY S FUEL PRE VLV OPEN S FUEL PRE VLV OPEN S FUEL PRE VLV CLSD S LOZ PUMP INLET LOZ PRE VALVE OPEN S FUEL PRE VLV CLSD S LOZ PUMP INLET BZ LOZ PUMP INLET	TRANSIENT 485 TO 530 TO 495 PSIG TRANSIENT 67 TO 62 TO 63 PSIG 200 PSIG TRANSIENT OSCILLATES 25.4 TO 28.3 PSIG OSCILLATES 25.4 TO 28.3 PSIG OSCILLATES 25.4 TO 28.3 PSIG OSCILLATES 25.4 TO 28.3 PSIG OSCILLATES 25.4 TO 28.3 PSIG DEC FROM 771 PSIG FOR 1.8 SEC STEADY AT 24.5 PSIG TO AMB /17 PSIG DEC FROM MAX TO AMB TRACE NOISY FOR 8.8 SEC @ MINUS 2.5 PSI TEMP INC DEACTIVATE DEC FROM 28.5 PSIG TO 12.7 PSIG DEC FROM 45 PSIG TO 29 PSIG DEC FROM 94 PSIG TO 29 PSIG
220-2 PIO14T ENGINE COMP AMB SEC 107-2 A1264D MSL TK MOVEMENT X AX DEC TO NINUS .270 INCHES 122-2 PIO04P B2 FUEL PUMP INLET TRACE STABLE NEAR D PSIG 208-3 PI280P SGG FUEL VLV INLET BEGAN RANDOM NOISE 107-3 A1266D MSL TK MOVEMENT Y AX DEC TO MINUS .050 INCHES 86 PI588X S TBN OVERSPEED TRIP DEACTIVATE	17.97	123-1	PIOOIP	BI LOZ PUMP IN	DEC FROM 52 PSIG TO 30 PSIG
220-2 P1014T ENGINE COMP AMB 107-2 A1264D HSL TK MOVEMENT X AX 122-2 P1004P B2 FUEL PUMP INLET 208-3 P1280P SGG FUEL VLV INLET 107-3 A1266D MSL TK MOVEMENT Y AX 86 P1588X S TBN OVERSPEED TRIP	20.67	220-2	P10141	ENGINE COMP AMB	FROM PLUS PEG TO 105.0 DEG F IN
122-2 PIOO4P B2 FUEL PUNP INLET 208-3 PI200P SGG FUEL VLV INLET 107-3 A1266D MSL TK MOVEMENT Y AX 86 PI588X S TBN OVERSPEED TRIP	20.67	220-2	P1014T	ENGINE COMP AMB	SEC TO MINIS JOID INCHES
208-3 PI280P SGG FUEL VLV INLET 107-3 A1266D MSL TK MOVEMENT Y AX 86 PIS88X S TBN OVERSPEED TRIP	20.87	122-2	A12640 P1004P	MSL TK MOVEMENT X AX B2 FUEL PUNP INLET	DEC 10 MINUS &ZTO INCHES TRACE STABLE NEAR 0 PSIG
107-3 A1266D MSL TK MOVEMENT Y AX 86 P1588X S TBN OVERSPEED TRIP	21.37	208-3	P1280P	SGG FUEL VLV INLET	BEGAN RANDOM NOISE
	22.87	107-3	A1266D P1588X		DEC TO MINUS .050 INCHES DEACTIVATE

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34.87	123-3	P1056P	S LO2 PUMP INCET	AND OF ALSO WE MORE DAG
35.87	213-1	H1140P	V HYD PUMP DISCH	INC FROM 1690 TO 4940 DATE
35.83	123-1	P1001P	BI LO2 PUMP IN	DEC PROM AD DATA TO D DATA
35.87	122-1	P1003P	BZ LOZ PUMP IN	CENTRAL SECTION OF THE SECTION OF TH
40.87	117-2	P1336T	S GAS GEN DISCH	INC FROM PEG NEG TO 44 DEG R
47.87	107-3	A1266D	MSL TK MOVEMENT Y AX	INC TO MINUS .022 INCHES
47.87	113-1	F1142P	S CTL PNEU REG OUT	BEGAN OSCILLATION
47.87	123-3	F1056P	S LO2 PUMP INLET	BEGAN RANDOM OSCILLATIONS
47.87	115-3	PlosoP	BI THRUST CHAMBER	OSCILLATES PLUS THEN PEGS MINUS
48.87	119-2	F1003P	FUEL TANK HELIUM	DEC SEG III TO II /22+9 PSIG/ IN 1948 SW
48.87	115-2	P1059P	B2 THRUST CHAMBER	
48.87	113-2	P1344P	S LO2 REG REF	BEGAN RANDOM NOISE
49.87	111-2	P1026P	B LO2 REG REF	OSCILLATES PLUS THEN PEGS MINUS
51.87	113-3	PIITTP	B LOZ START TANK REG	RANDOM OSCILLATIONS
52.87	216-2	F1124P	S TK HE BTL DISCH	BEGAN OSCILLATION
52.87	111-1	F1125P	B CTL PNEU REG	BEGAN OSCILLATION
52.87	216-1	F1145P	S CTL HE BTL DISCH	BEGAN OSCILLATION
52.87	212-3	HILBIT	S HYD PUMP DISCH	INC 20 DEG F
33.37	109-2	P1235P	VERN LOZ TK REG OUT	BEGAN RANDOM TRANSIENTS
54.37	110-2	P1236P	VERN FUEL TANK REG OUT	BEGAN RANDOM OSCILLATIONS
72.87	107-3	A1266D	MSL TK MOVEMENT Y AX	DEC TO MINUS .090 INCHES
38.87	221-1	E1027V	PROP CONTROL INPUT	ERRATIC TRACE
56.37	220-2	P10147	ENGINE COMP AMB	TRANSIENT 75.5 TO 97.6 TO 70.5 DEG F
	න		SPARE	DEACTIVATE
	ው		SPARE	ACTIVATE
	88		SPARE	DEACTIVATE

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DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	PRE START STEADY 1900 PS1G	DEACTIVATE	DEACTIVATE	DEACTIVATE
SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	SPARE	V HYD PUMP DISCH	APS HYD UNDER PRESS	B COF RELAY LOCKIN	B LUBE TANK PRESD SW
																						H1140P	H1066X	PIOTZX	P1129X
34	37	62	76	89	46	80	96	16	ۍ 30	111	223	119	120	123	124	125	142	143	144	145	146	213-1	61	9	4

CONTIDERTAL

P1148X B FUEL VLV CLOS CTL SOL DEACTIVATE P1150X B FUEL VLV CLOS CTL SOL DEACTIVATE P1154X TCC B ENGINE COF SW DEACTIVATE P1155X GBSERVER CUTOFF DEACTIVATE P1155X B1 TBN OVRSPEED TRIP DEACTIVATE P1155X B2 TBN OVRSPEED TRIP DEACTIVATE P1155X B2 TBN OVRSPEED TRIP DEACTIVATE P1155X B1 LUBE TK PRESS COF DEACTIVATE P1155X B1 LUBE TK PRESS COF DEACTIVATE P1164X TCC FUEL S T FULL LT DEACTIVATE P1195X B1 ROUGH COMB COF DEACTIVATE P1195X B1 FUEL VLV OPEN MSW DEACTIVATE P1195X B1 FUEL VLV OPEN MSW DEACTIVATE P1200X SUSTAINER PUV SOL E DEACTIVATE P1201X SUSTAINER PUV CLSD MSW DEACTIVATE P1203X FUEL PUV OPEN MSW DEACTIVATE P1203X S FUEL PUV OPEN MSW DEACTIVATE P1203X S FUEL PUV OPEN MSW DEACTIVATE P12199X B1 OBSERVER CUTOFF DEACTIV	P1136X P1166X P1165X P1166X	B IGN DETR DELAY COF B LUBE TNK PRESS SOL BGG VLV OPEN CTL SOL BGG VLV CLOS CTL SOL BGG VLV OPEN MSW	DEACTIVATE DEACTIVATE DEACTIVATE DEACTIVATE DEACTIVATE
DESERVER CUTOFF BI TBN OVRSPEED TRIP BZ TEN OVRSPEED TRIP PREP INCOMPLETE COF B LUBE TK PRESS COF TCC FUEL S T FULL LI BI ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF BZ FUEL VLV OPEN MSW BZ FUEL VLV OPEN MSW SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF #3 OBSERVER CUTOFF	× × ×		DEACTIVATE DEACTIVATE
BI TBN OVRSPEED TRIP B2 TBN OVRSPEED TRIP PREP INCOMPLETE COF B LUBE TK PRESS COF TCC VERN ENG COF SW TCC FUEL S T FULL LI BI ROUGH COMB COF B2 ROUGH COMB COF B2 ROUGH COMB COF B2 ROUGH COMB COF B3 ROUGH COMB COF B3 ROUGH COMB COF B3 ROUGH COMB COF B3 ROUGH COMB COF B3 ROUGH COMB COF B4 ROUGH COMB COF B5 FUEL VLV OPEN MSW SUSTAINER PUV SOL E S FUEL PUV CLSO MSW B1 OBSERVER CUIOFF B2 OBSERVER CUIOFF B3 OBSERVER CUIOFF	X X	TCC B ENGINE COF SW OBSERVER CUTOFF	DEACTIVATE
B LUBE TK PRESS COF ICC VERN ENG COF SW TCC FUEL S T FULL LI BI ROUGH COMB COF BZ ROUGH COMB COF BI FUEL VLV OPEN MSW BZ FUEL VLV OPEN MSW SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUIOFF #2 OBSERVER CUIOFF	56X	BI TBN OVRSPEED TRIP B2 TBN OVRSPEED TRIP	DEACTIVATE DEACTIVATE
B LUBE IK FRESS COF TCC VERN ENG COF SW TCC FUEL S T FULL LI BI ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF BZ ROUGH COMB COF SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	58X	PREP INCOMPLETE COF	DEACTIVATE
BI ROUGH COMB COF BI ROUGH COMB COF BI FUEL VLV OPEN MSW BI FUEL VLV OPEN MSW SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF #3 OBSERVER CUTOFF	% % X X	6 LUBE TK PRESS COF TCC VERN ENG COF SW	DEACTIVATE
BI ROUGH COMB COF BZ ROUGH COMB COF BI FUEL VLV OPEN MSW BZ FUEL VLV OPEN MSW SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	86X	TCC FUEL S T FULL LT	DEACTIVATE
B1 FUEL VLV OPEN MSW B2 FUEL VLV OPEN MSW SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	92X 03X	BI ROUGH COMB COF	DEACTIVATE
SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	X 7 6	BI FUEL VLY OPEN MSW	DEACTIVATE
SUSTAINER PUV SOL F SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	X26.	82 FUEL VLY OPEN MSW	DEACTIVATE
SUSTAINER PUV SOL E S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	X00	SUSTAINER PUV SOL F	DEACTIVATE
S FUEL PUV OPEN MSW S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	o1x	SUSTAINER PUV SOL E	DEACTIVATE
S FUEL PUV CLSD MSW #1 OBSERVER CUTOFF #2 OBSERVER CUTOFF #3 OBSERVER CUTOFF	02X	S FUEL PUV OPEN MSW	DEACTIVATE
#1 OBSERVER CUTOFF #2 OBSERVER CUTOFF	XEO	S FUEL PUV CLSD MSW	ACTIVATE
#2 OBSERVER CUTOFF	19X	#1 OBSERVER CUTOFF	DEACTIVATE
#3 OBSERVER CUTOFF	20X		DEACTIVATE
	21X	OBSERVER	DEACTIVATE

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152	P1222X	#4 OBSERVER CUTOFF	DEACTIVATE
159	P1223X	#5 OBSERVER CUTOFF	DEACTIVATE
154	P1224X	#6 OBSERVER CUTOFF	DEACTIVATE
155	P1225X	#7 OBSERVER CUTOFF	DEACTIVATE
156	P1226X	#8 OBSERVER CUTOFF	DEACTIVATE
151	P1227X	#9 OBSERVER CUTOFF	DEACTIVATE
158	P1228X	#10 OBSERVER CUTOFF	DEACTIVATE
159	P1229X	#11 OBSERVER CUTOFF	DEACTIVATE
160	P1230X	#12 OBSERVER CUTOFF	DEACTIVATE
147	P1231X	OBSERVER CUTOFF N : ANK	DEACTIVATE
148	P1232X	OBSERVER CUTOFF S TANK	DEACTIVATE
78	P1335X	SGG VALVE CLSD MSW	ACTIVATE
10	P1379X	APS ARM	DEACTIVATE
e e	P1381X	APS RUR	DEACTIVATE
14	P1382X	APS IGNITION	DEACTIVATE
e) m	P1383X	APS COMPOSIT VLV SOL	DEACTIVATE
16	P1386X	APS READY TO COMMIT	DEACTIVATE
17	P1388X	APS COMMIT	DEACTIVATE
18	P1390X	APS SPEED SHUTDOWN	DEACTIVATE
70	P1429X	TCC RELEASE SWITCH	DEACTIVATE
85	P1438X	ROUGH COMB COF S	DEACTIVATE
89 101	P1441X	B IGN STAGE TIMER-DO	DEACTIVATE
7	P1446X	B FUEL PRE VLV CLSD	DEACTIVATE
19	P1499X	SGG VLV OPEN MSW	DEACTIVATE
82	P1515X	VERN SRT DY COF	DEACTIVATE
40	PISIGX	VERN STRT DY COF THR	DEACTIVATE

COMEDENTIAL

DEACTIVATE DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	ACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	DEACTIVATE	OPERATED EACH 1.5 SEC
PRE START READY	S FUEL TK PRESS SOL	S LUBE TNK PRESS SW	S GG VLY OPEN CTL	S HYD PRESS SW	BOOSTER ENG CUTOFF	SUSTAINER ENG CUTOFF	TCC SUSTAINER COF SW	SEG VLV CLOSING SOL	HOLD DN PRE-LEASE	S LUBE TK PRESS COF	PROGRAMER RUN TIME	BOOSTER COF DISCRETE	JETTISON BOOSTER SIG	PRES VERN TKS DISC	SUSTAINER COF DISC	PRE-ARM DISCRETE	PRE-ARM PRGR OTP	VERNIER COF DISCRETE	RLS IN-FLIGHT DISCON	RELEASE NOSE CONE	FIRE RETRO-ROCKET	VIB PRINTER TIME
P1561X P1575X	P1584X	PISESX	P1587X	PISSIX	P1592X	P1593X	P1594X	P1595X	P1596X	P1597X	S1235X	S1236X	S1238X	S1239X	S1241X	\$1243X	S1244X	S1245X	51247X	51248X	\$1249X	ST215X
103	6 49	65	77	104	105	106	109	116	118	66	126	127	129	130	132	134	135	136	138	139	140	122

APPENDIX E

PHOTOGRAPHS OF DAMAGE

RUN S2-212-B4-01

CONVAIR ASTRONAUTICS



PHOTO No. I SUSTAINER THRUST CHAMBER

CONVAIR ASTRONAUTICS

SUST IST STAGE TURBINE WHEEL -

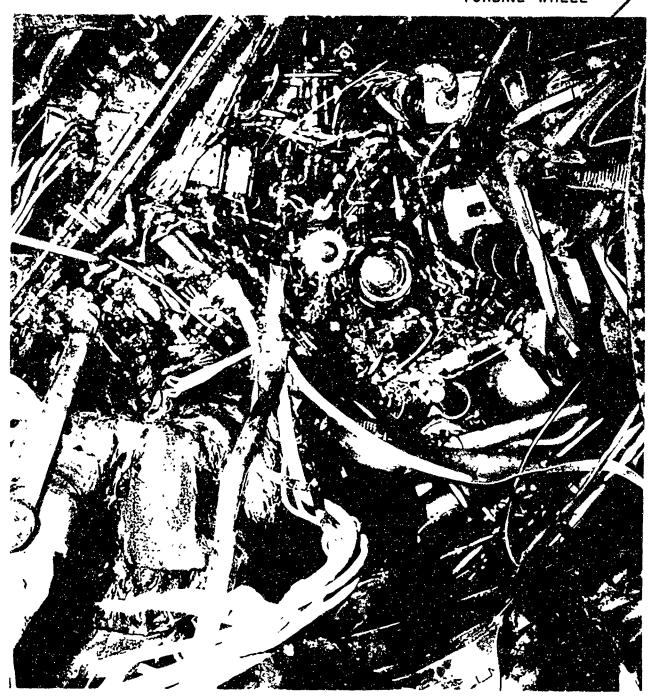


PHOTO No. 2
VIEW BETWEEN BI& SUSTR THRUST CHAMBERS

CONVAIR ASTRONAUTICS



PHOTO No. 3
THRUST SECTION QUARDS III & IV

CONVAIR ASTRONAUTICS



PHOTO No.4
BOOSTER LUBE OIL TANK

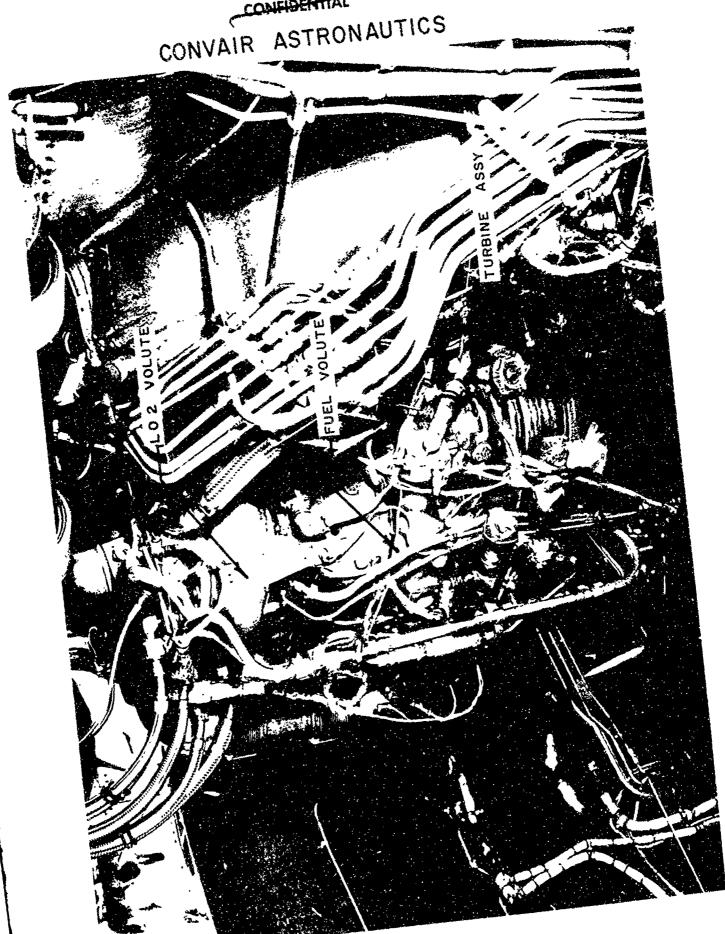


PHOTO No. 5 TURBO PUMP ASSEMBLY SUSTR.

CONVAIR ASTRONAUTICS

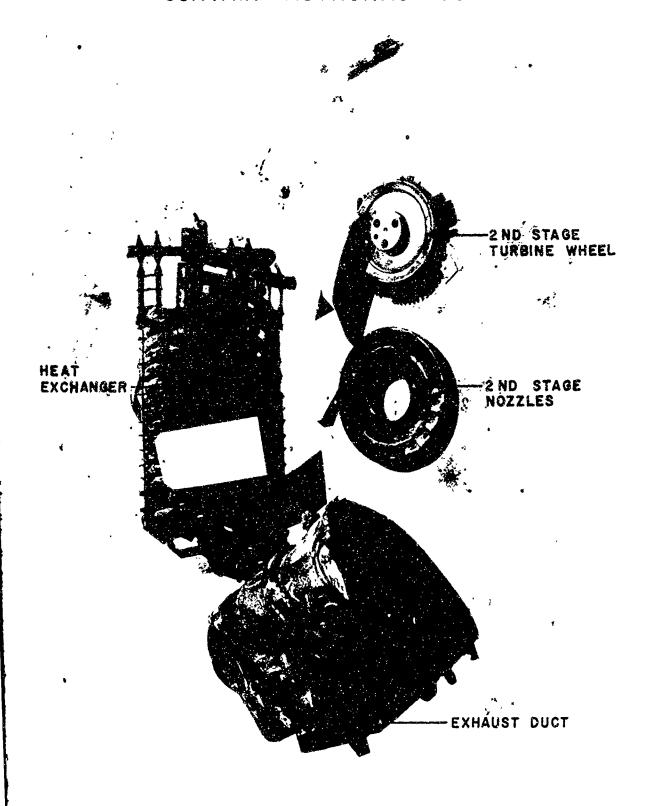


PHOTO No. 6
MAJOR SUSTAINER ENGINE PARTS
EJECTED BY THE EXPLOSION

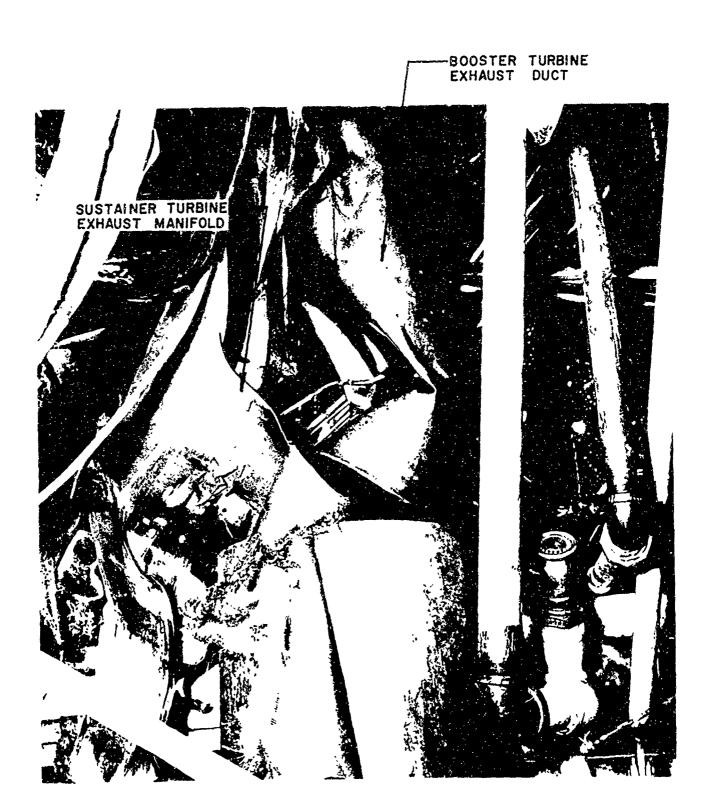


PHOTO No. 7
BOOSTER TURBINE EXHAUST &
SUSTAINER TURBINE EXHAUST MANIFOLD

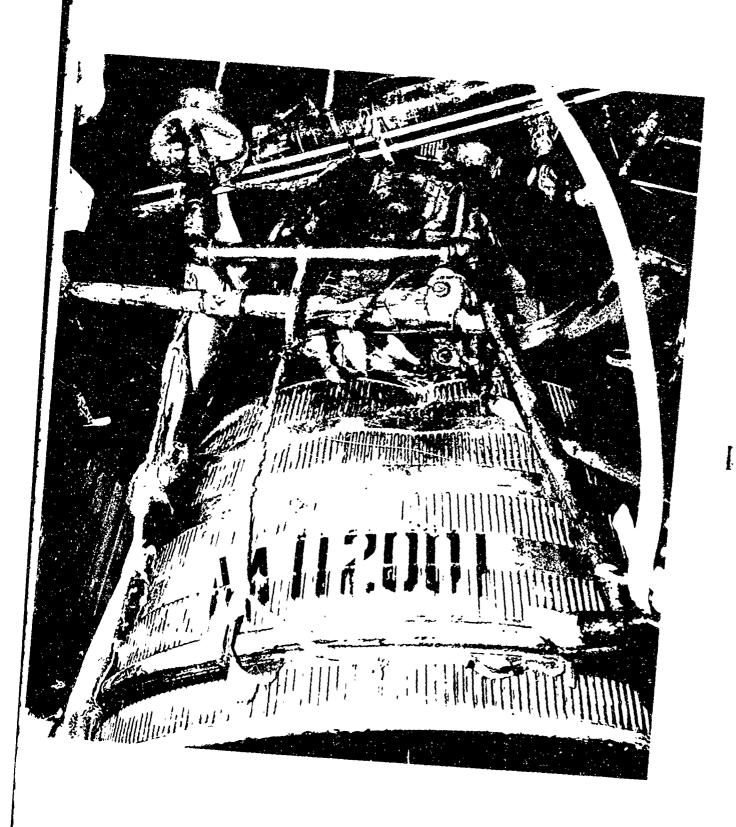


PHOTO No. 8 BI THRUST CHAMBER



PHOTO No. 9
INTERIOR OF BI CHAMBER

CONVAIR ASTRONAUTICS

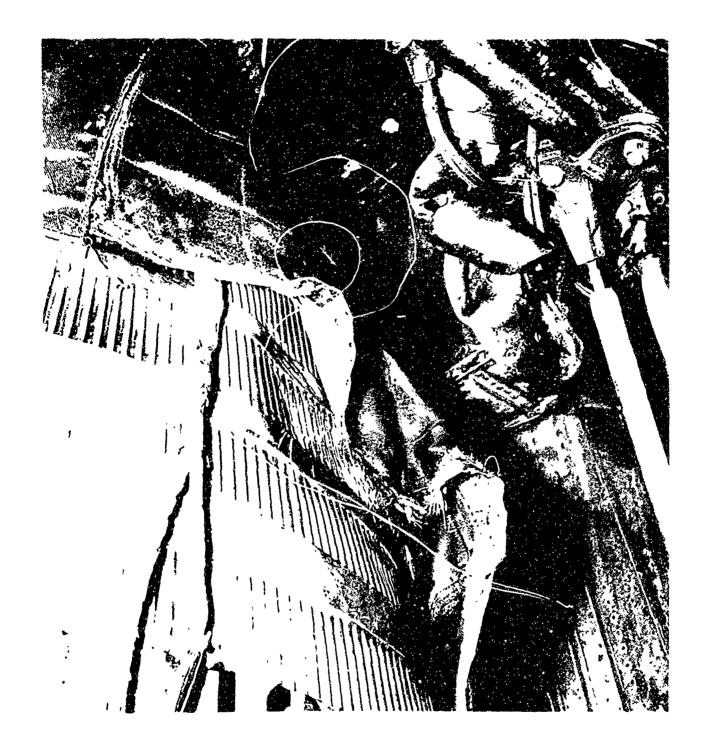


PHOTO No.10 B2 THRUST CHAMBER

CONVAIR ASTRONAUTICS



PHOTO No. 11 INTERIOR OF B2 CHAMBER

CONVAIR ASTRONAUTICS

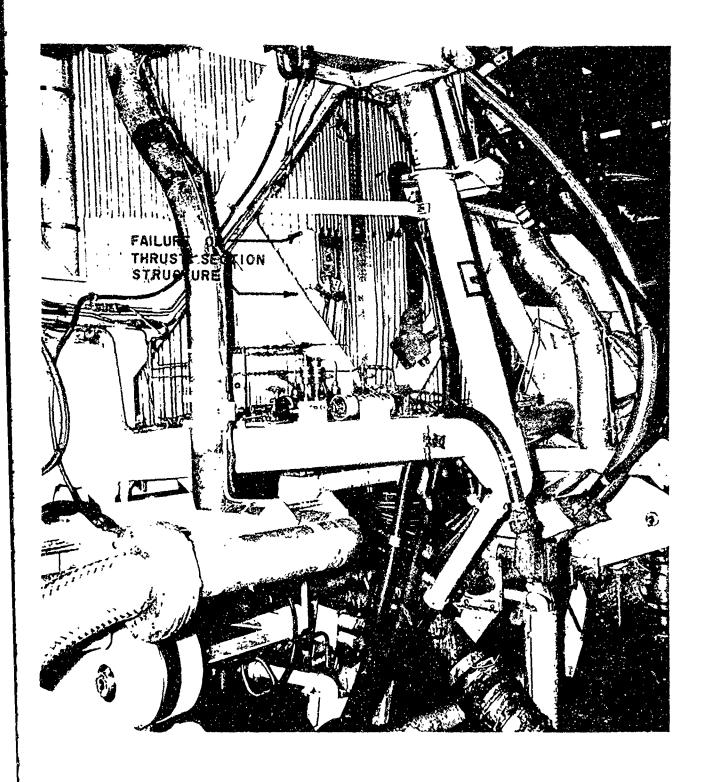


PHOTO No. 12
EXTERIOR SKIRT DAMAGE
QUAD IV AND EJECTED UMBILICALS



PHOTO No. 13 PURGE RISE OFF PANEL



PHOTO No. 14
FAIRING DAMAGE INTERIOR OF QUAD I

-CONTIDENTIAL

CONVAIR ASTRONAUTICS

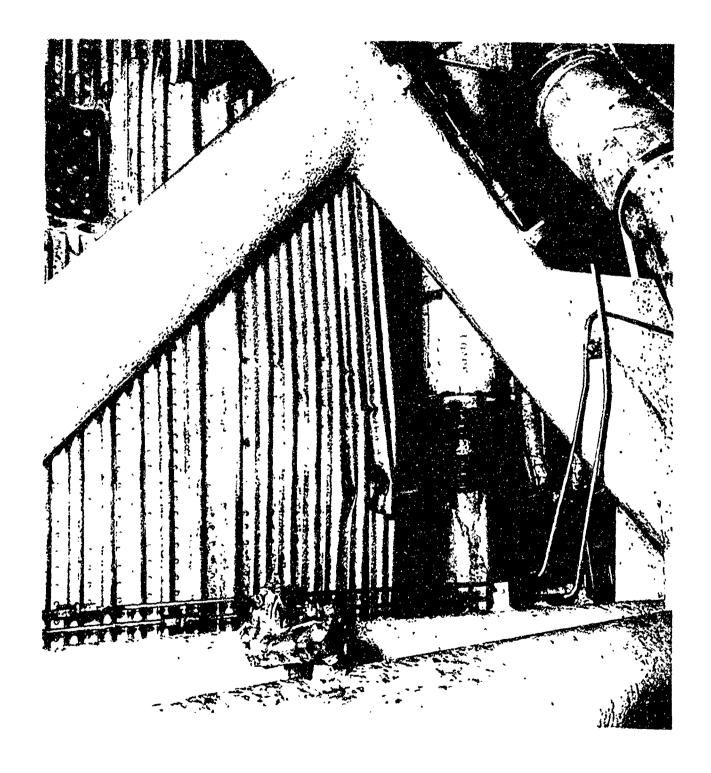


PHOTO No.15
FAIRING DAMAGE QUAD IV

CONVAIR ASTRONAUTICS

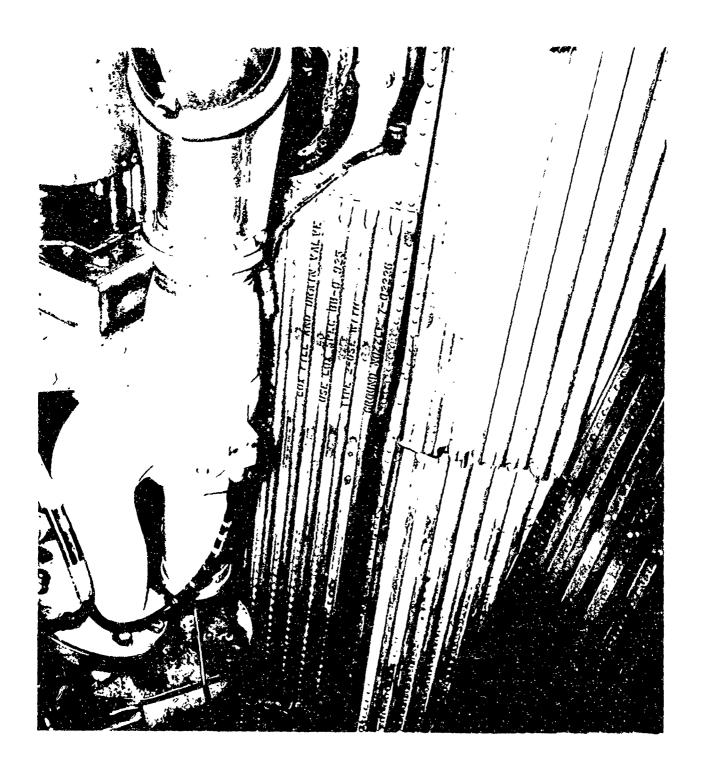


PHOTO No. 16
FAIRING DAMAGE QUAD IV



PHOTO No. 17
SUSTAINER GAS GENERATOR
AS REMOVED FROM MISSILE
CONFIDENTIAL

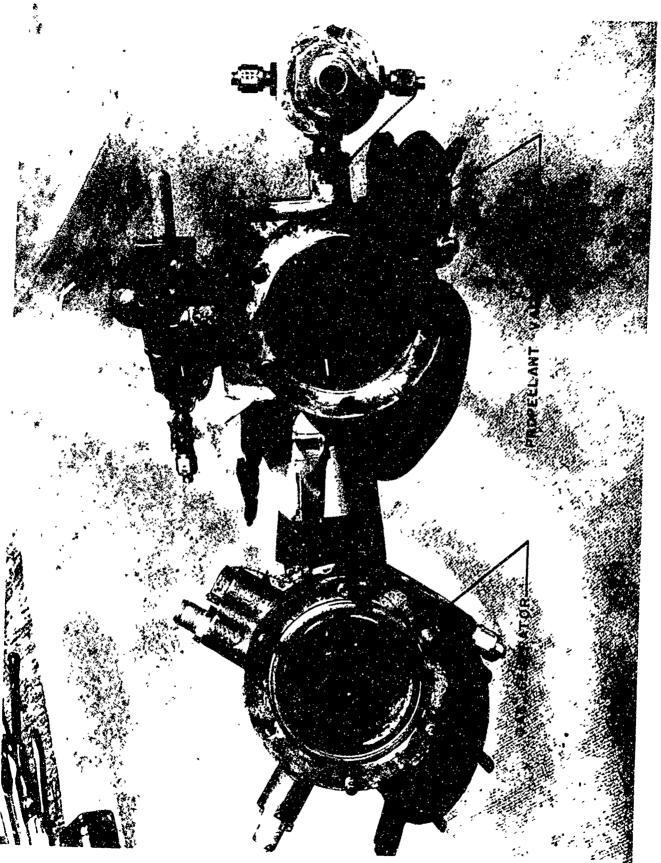


PHOTO No, 18
SUSTAINER PROPELLANT VALVE
ASSEMBLY REMOVED FROM GAS GENERATOR

(1

COLIFIDENTIAL

CONVAIR ASTRONAUTICS

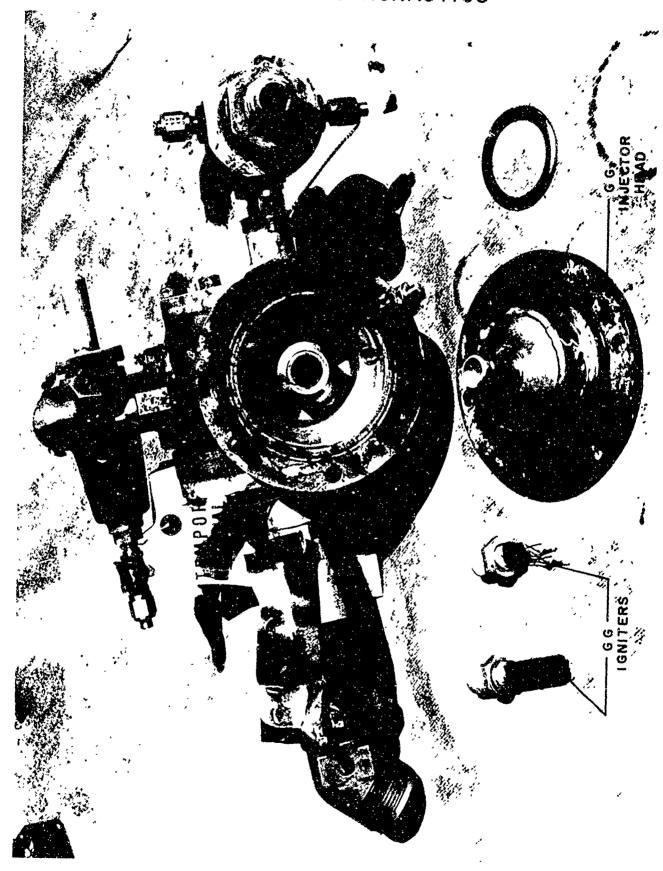


PHOTO No.19
PROPELLANT VALVE ASSEMBLY
WITH INJECTOR HEAD REMOVED

CONFIDENTIAL CONVAIR ASTRONAUTICS

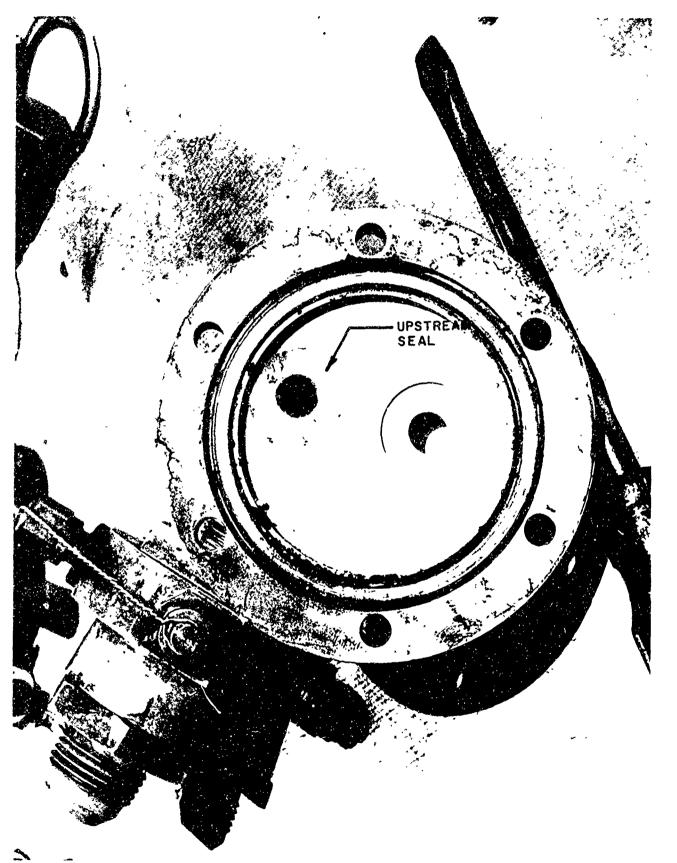


PHOTO No. 20 LO2 BLADE VALVE COVER PLATE SHOWING CRACKED UPSTREAM SEAL

CONVAIR ASTRONAUTICS

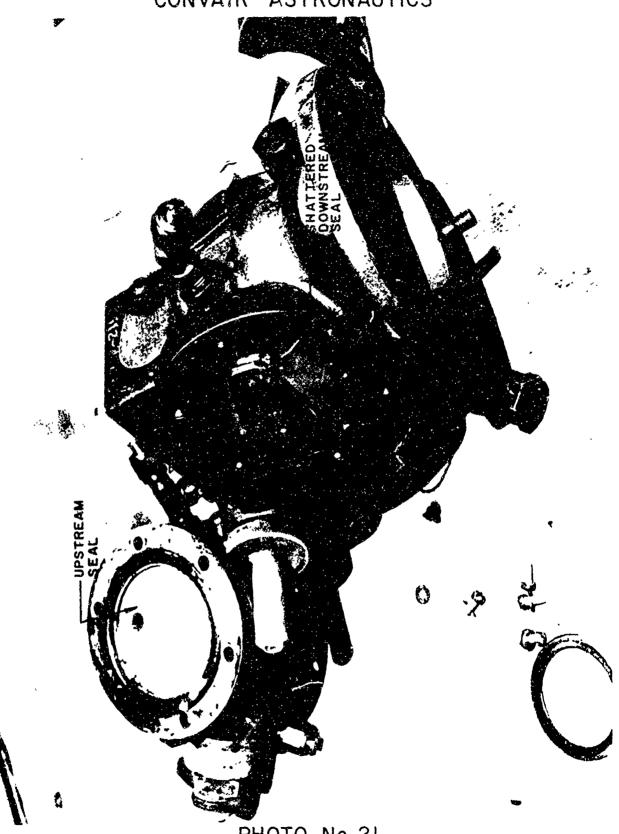


PHOTO No. 21

LO 2 BLADE VALVE SHOWING

SHATTERED DOWNSTREAM SEAL AND

POSITION OF VALVE WHEN DISASSEMBLED

VIEW I

CONVAIR ASTRONAUTICS

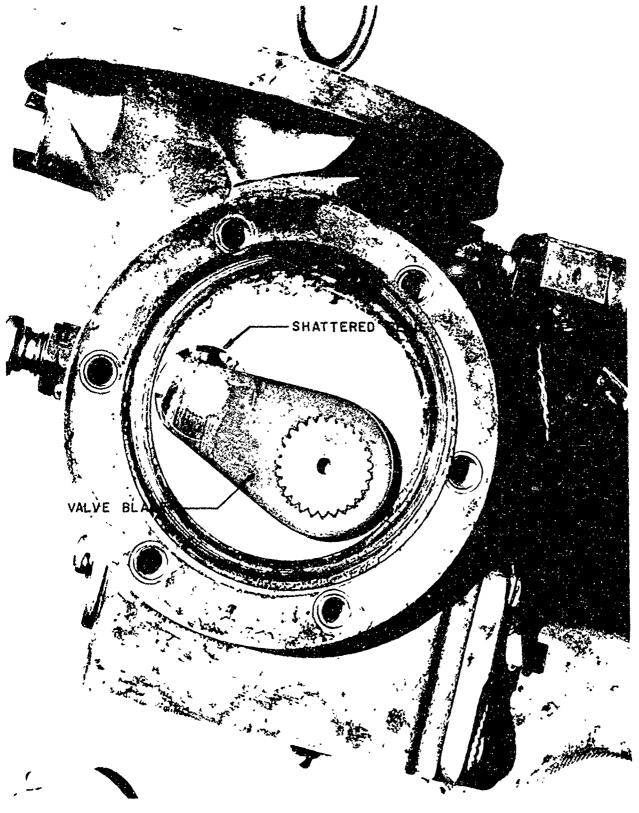


PHOTO No. 22

LO 2 BLADE VALVE SHOWING

SHATTERED DOWNSTREAM SEAL AND
POSITION OF VALVE WHEN DISASSEMBLED

VIEW 2

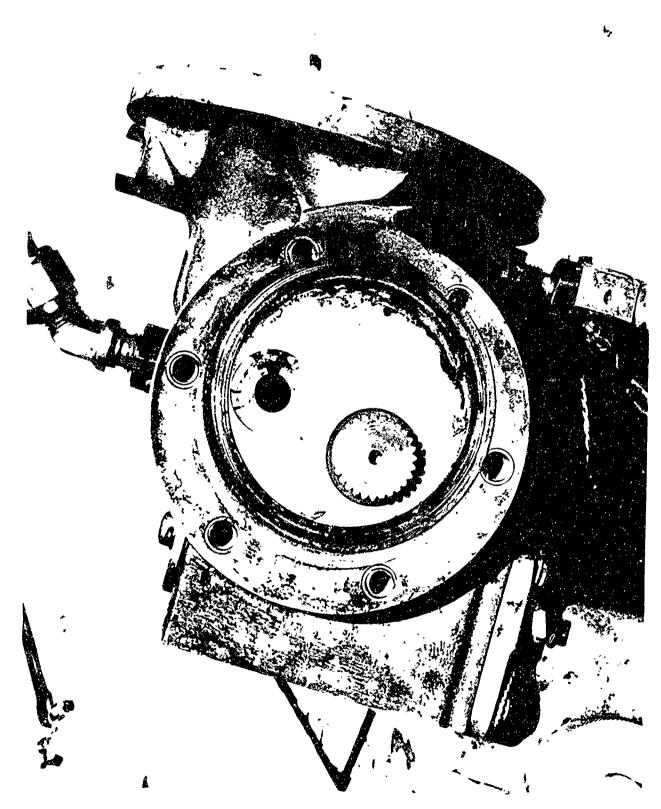


PHOTO No.23 LO2 BLADE VALVE DOWNSTREAM SEAL WITH BLADE REMOVED

-CONFIDENTIAL- -

CONVAIR ASTRONAUTICS



PHOTO No. 24 LO2 BLADE VALVE DOWNSTEAM SEAL

CONVAIR ASTRONAUTICS



РНОТО No. 25 LO2 BLADE VALVE UPSTREAM SEAL

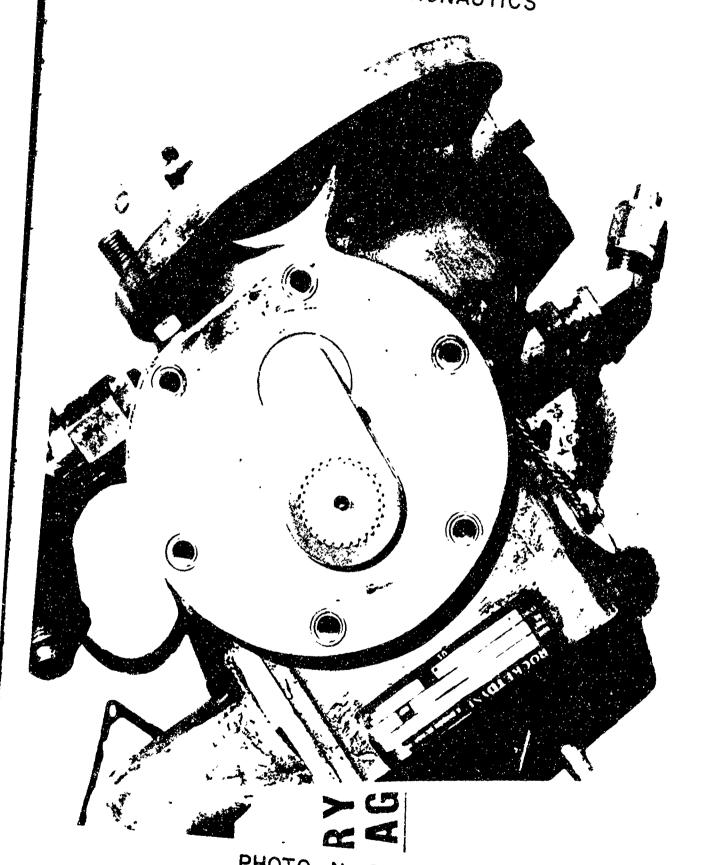


PHOTO No. 26 FUEL BLADE VALVE SHOWING DOWNSTREAM SEAL INTACT

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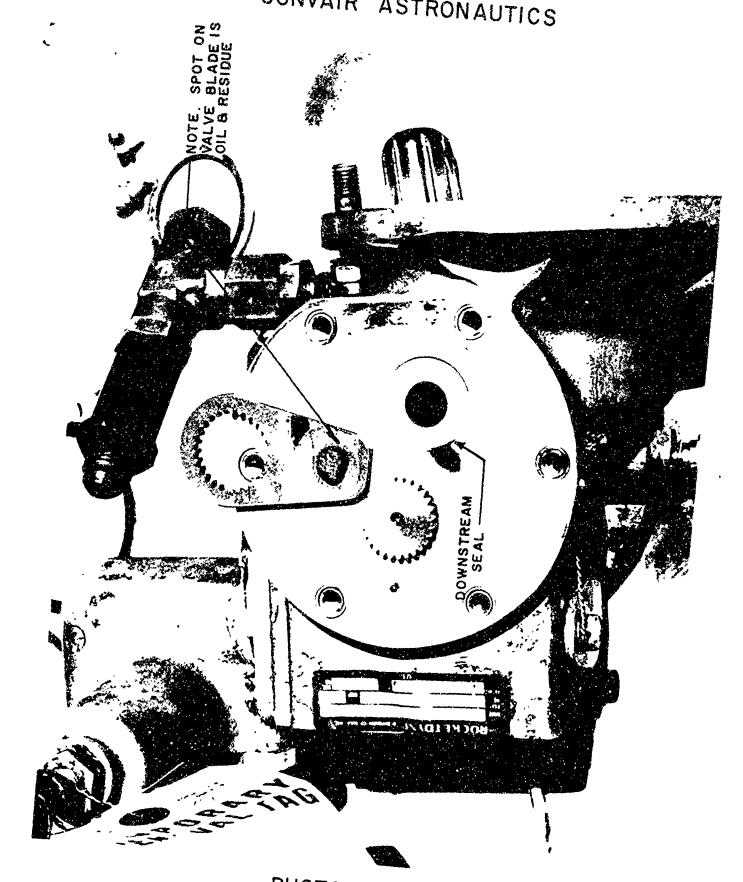


PHOTO No. 27 FUEL BLADE VALVE DOWNSTREAM SEAL WITH BLADE REMOVED AND TURNED OVER

CONTIDENTAL ...

CONVAIR ASTRONAUTICS

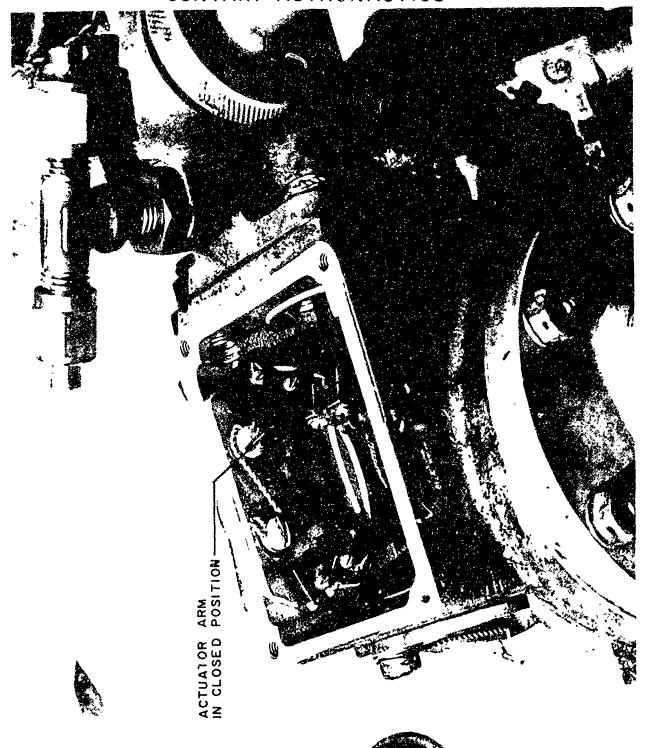


PHOTO No. 28
SUSTAINER GAS GENERATOR
PROPELLANT VALVE ASSEMBLY AS
DISASSEMBLED

T.	
•	
	APPENDIX F
	ROCKETDYNE INVESTIGATION REPORT
/re Us	S2-212-B4-01
e.	
& V	

FINAL ACCIDENT REFORM RUN S2-212-B4-01

LEM 844-1014 30 June 1958

TO:

M. A. McClure, 596-42, Canoga

FROM:

н. L. Conrad, 596-44, Canoga

SUBJECT:

Accident Report Missile 1B (Engine S,'N NA112001) at Sycamore

Canyon Test Facility

At 16:38 hours on 18 June 1958, an explosion occurred in the turbine of the Sustainer engine (S/N NA222007) installed in Missile 1B as part of engine assembly S/N NA112001. This explosion caused considerable damage to the lower boattail structure, Ecoster chambers, Booster power package assembly, and the Sustainer engine assembly. Apparent cause of the explosion was failure of the Sustainer gas generator blade valve LO₂ seel at cutoff on the previous run.

The test in which the explosion occurred was the twelfth scheduled test on this missile and the fourth attempt to complete the first run of the Block II series of tests. The run was scheduled to be 100 seconds Booster, 194 seconds Sustainer, and 220.5 seconds of Vernier engine operation. Countdown and start appeared normal. Approximately 0.04 seconds after the gas generator igniters were signalled to fire, the explosion occurred. The ensuing fire was extinguished in approximately twelve (12) seconds by using water and CO₂.

Examination of Records

Examination of all records on this run and the previous run revealed the following:

- 1. Normal conditions prior to start and during the previous run.
- 2. On the previous run, the Sustan. " gas generator probe had been burned off. Indications were that this had been caused by a cutoff temperature spike. (The chart was regged at 1800°F). Momentary temperature spikes had occurred at cutoff on all previous runs. No pressure surge could be detected because the LO2 injection manifold pressure and gas generator chamber pressure charts were inoperative. The gas generator system was examined externally for signs of high temperature prior to Run 12 and the results were negative.



IEM 11-101:

30 June 1950 Inje 2

Examination of Records (Continued)

- 3. About his seconds after dutefor out the provious run (approximately five feet of oscillograph paper), the LO. Nowhether indicated intermittent flow until the recentor was turned out.
- The escillagramic trace indicated LOg Thry to the Sustainer gas generator on this run prior to scart.
- 5. The Sustainer as generator discharge temperature chart was regard down scale prior to start of this run

Examination of Harluare

Examination of the Sustainer gas & . . r after the explosion revealed a detonation or severe pressure surge had recurred in the LOX injector manifold. Further, the LOT seal was found to be shattered and the outline of the valve blade was impressed on the lack-up plate for the seal.

Erobable Couse

The probable on se and events leading up to the explosion is believed to be as follows:

- 1. The Sustainer was generator LOo blad, velve seal was shattered presumably at cutoff on the previous run by a sharp pressure surge or detonation in the LOo injector manifold of the gas memerator as indicated by the following:
 - a) The was generator injector was with downward and the manifold was bound upward.
 - b' Trons perenttor plade valve has in the closed position.
 - e) Temporature splits and possible precisions since at outoff on the provides in a (i.g. ressure information respondently verify pressure single).
 - 1) LOg Nouse je industrialni i i i dele in previous mun and prior to statule of this name.

The sum compatibility of publishing the line equate pure at eathful This ait ation of the male at ation of the male at ation of the male at ation of the mission was in the embedding the published of the mission of the ation of the ation of the ation of the finite ation.

2. The failed most remarked in , or the control of the following to make continuous control of the control of t

FINAL ACCIDENT REPORT RUN S2-212-B4-01

> LEM 844-1014 30 June 1958 Page 3

Action Taken

The following action has been taken to minimize the possibility of this type of accident happening in the future:

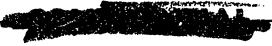
- 1. A Field Service Bulletin has been written to re-emphasize ROCKETDYNE's recommended purge pressures and sequencing.
- 2. Recommend that cutoff temperature spikes on future tests be carefully evaluated to insure that no contamination of the gas generator LO₂ injector manifold has occurred.
- 3. Gas generator flowmeter and discharge temperature records be checked before and after each run for signs of LO₂ leakage.
- 4. The gas generator exhaust systems should be checked after LO₂ tanking for signs of LO₂ vapors.

A complete and detailed accident report is being prepared as a joint effort of Convair, Air Force, Ramo-Wooldridge and ROCKETDYNE representatives at Sycamore Canyon test site.

s/_		
	H. L. Conrad,	
	Flight Support	Unit
	ATLAS Engines	

APPROVED:

H. Diem, Supervisor Flight Support Unit ATIAS Engines



NCLASSIFIED

ROCKETDYNE

FAILURE ALALYSIS REPORT

A DIVISION OF NORTH AMERICAN AVIATION, INC.

1. Report No. 177666

2. Date of Analysis 3 Test No. 23 July 1958

4A. Facility 4B Location Rocketdyne A8

5. Failed Item P/N 9512-44185-51

6. Failed Item S/N P-086

7. Failed Item Name 8. F/1 Type or Sus G.G. Assy

Model

- 9. HISTORY OF TROUBLE (NOTED FROM ITEM 26.1 ON F.C.D.R): On 18 June 1958, captive firing test No. 11 (TE-11) was performed at the Sycamore Canyon installation. After 2.34 seconds of mainstage start, the Gas Generator squibbs fired, followed by an explosion in the Turbine and Turbine Exhaust system. This explosion resulted in almost complete destruction of the sustainer engine. Extensive damage was also inflicted on the booster engine. In reviewing the test records on the sustainer engine, it was disclosed that a steady oxidizer flow was evident in the Gas Generator for 80 seconds prior to firing the Vernier squibbs. Flow rates recorded were .3 lbs/sec under tank head pressure and .51 lbs/sec at pressurization. Thermo-couple readings at the hot gas duct had dropped 30° below ambient temperature.
- 10. ANALYSIS PROCEDURE AND RESULTS: Disassembly of the Gas Generator disclosed the G.G. blade valve to be in the correct closed position and the following damaged detail parts were noted:
 - 1. Shattered Oxidizer port seal.
 - 2. Radially cracked pressure pad.
 - Oxidizer inlet cover place with gate impression at the edge of the pad cavity
 - \dot{l}_{i} . Dull (not abrasive) surface bearing the outline of the port seal bore on the Lox blade.
 - 5. Partially burned silicone "O" ring.
 - 6. Bits of grey ash and hard matter within the oxidizer cover cavity.
 - 7. I.D. of the fuel seal locally burned in one area.

Further examination revealed that the injector plate yielded convexly on the normally flat surfaces. The injector face had bulged .068 inches at its maximum point. The flange surface took a permanent deflection of .020 inches. Spectro-analysis proved the grey ash and hard matter to be part of the burned silicone "O" ring. The oxidizer port seal was inspected under a magnifying instrument and no obvious wear or mars were evident.

- 11. CONCLUSIONS AS TO CAUSE OF FAILURE:
 - It is an established fact that the oxidizer seal in the G.G. blade valve was leaking prior to the major explosion of the engine. Conclusions that the seal was shattered by a detonation car only be derived from what evidence is presented in test records and past experience of similarly shattered oxidize: port seals. Test run prior to X day had shown intermittent G.G. oxidizer flow and a prolonged temperature spike after G.C. cutoff. Records, therefore, imply that the oxidizer port seal had failed in the previous firing after cutoff
- 12. RECOMMENDATIONS FOR PREVENTING RECURRENCE AND ACTION TAKEN: R & D experience have had only 3 instances where exidizer seals were shattered or cracked as a result of detonations internal to the G.G. Assy. or adjacent downstream hardware. Normal runs on this type G.G. have shown temperature spikes after cutoff (not to be common) except where purging is inadequate. Due to oxidizer seal leakage frequently being very low and seal cracking rare, no design change is contemplated in this area of the valve assembly. Malfunction studies will purge procedure is under be extended should this consideration.